

Standard Heat Treatments for Fabrication Processes

ASME Code for Pressure Piping, B31

AN AMERICAN NATIONAL STANDARD



**The American Society of
Mechanical Engineers**

Standard Heat Treatments for Fabrication Processes

ASME Code for Pressure Piping, B31



**The American Society of
Mechanical Engineers**

Two Park Avenue • New York, NY • 10016 USA

Date of Issuance: May 15, 2018

The next edition of this Standard is scheduled for publication in 2021.

ASME issues written replies to inquiries concerning interpretations of technical aspects of this Standard. Interpretations are published under <http://go.asme.org/Interpretations>. Periodically certain actions of the ASME B31 Committees may be published as Cases. Cases are published on the ASME website under the Committee Pages at <http://go.asme.org/B31committee> as they are issued.

Errata to codes and standards may be posted on the ASME website under the Committee Pages to provide corrections to incorrectly published items, or to correct typographical or grammatical errors in codes and standards. Such errata shall be used on the date posted.

The B31 Committee Pages can be found at <http://go.asme.org/B31committee>. The associated B31 Committee Pages for each code and standard can be accessed from this main page. There is an option available to automatically receive an e-mail notification when errata are posted to a particular code or standard. This option can be found on the appropriate Committee Page after selecting "Errata" in the "Publication Information" section.

ASME is the registered trademark of The American Society of Mechanical Engineers.

This code or standard was developed under procedures accredited as meeting the criteria for American National Standards. The Standards Committee that approved the code or standard was balanced to assure that individuals from competent and concerned interests have had an opportunity to participate. The proposed code or standard was made available for public review and comment that provides an opportunity for additional public input from industry, academia, regulatory agencies, and the public-at-large.

ASME does not "approve," "rate," or "endorse" any item, construction, proprietary device, or activity.

ASME does not take any position with respect to the validity of any patent rights asserted in connection with any items mentioned in this document, and does not undertake to insure anyone utilizing a standard against liability for infringement of any applicable letters patent, nor assume any such liability. Users of a code or standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, is entirely their own responsibility.

Participation by federal agency representative(s) or person(s) affiliated with industry is not to be interpreted as government or industry endorsement of this code or standard.

ASME accepts responsibility for only those interpretations of this document issued in accordance with the established ASME procedures and policies, which precludes the issuance of interpretations by individuals.

No part of this document may be reproduced in any form,
in an electronic retrieval system or otherwise,
without the prior written permission of the publisher.

The American Society of Mechanical Engineers
Two Park Avenue, New York, NY 10016-5990

Copyright © 2018 by
THE AMERICAN SOCIETY OF MECHANICAL ENGINEERS
All rights reserved
Printed in U.S.A.

CONTENTS

Foreword	v
Committee Roster	vi
Correspondence With the B31 Committee	viii
1 Introduction	1
2 Glossary	1
3 Temperature Measurement	1
4 Temperature Control	2
5 Welding Preheat	3
6 Postweld Heat Treatment (PWHT)	4
7 Postforming and Material Heat Treatments	6
8 Alternatives and Exemptions to Preheat and PWHT Requirements	9
Nonmandatory Appendices	
A Recommendations for the Proper Use of Thermocouples	10
B Recommendations for Control of Narrow Temperature Range Heat Treatments: Local Heat-Treatment Methods	11
C Branch Connection Examples	26
D Temper Bead Method Alternative to PWHT	28
E Fracture Mechanics Alternative to PWHT	29
Figures	
B-3.1-1 Definition of Terms for Local Circumferential Band Heating of Pipe Weld	12
B-3.1-2 Definition of Terms for Local Circumferential Band Heating of Branch Connection to Pipe Attachment Weld	13
B-5.2-1 Location of Thermocouples (Monitoring and Control) for Pipe Sizes Less Than NPS 6 (150 DN) and One Control Zone	15
B-5.2-2 Location of Thermocouples (Monitoring and Control) for Pipe Sizes NPS 6 (DN 150) Up to and Including NPS 12 (DN 300) and Two Control Zones	16
B-5.2-3 Location of Thermocouples (Monitoring and Control) for Pipe Sizes NPS 14 (DN 350) Up to and Including NPS 30 (DN 750) and Four Control Zones	17
B-5.2-4 Location of Monitoring Thermocouples for Branch Nozzle or Attachment Welds	18
B-5.3-1 Example of One Approach When the Heated Band From a Weld Requiring PWHT Intersects a Weld Not Requiring PWHT	20
C-1 Typical Branch Attachment Details That May Be Used to Calculate Control Thickness	26
C-2 Typical Integrally Reinforced Outlet Fitting Branch Connection Details That May Be Used to Calculate Control Thickness	27
Tables	
5.1-1 Preheat Temperature	3
6.1.1-1 Postweld Heat Treatment	5

6.1.1-2	Alternate Postweld Heat Treatment Requirements for Carbon and Low-Alloy Steels, P-Nos. 1 and 3	6
6.1.1-3	Exemptions to Mandatory Postweld Heat Treatment	7
6.2-1	Approximate Lower Transformation Temperatures	9
B-5.1-1	Requirements for Control Zones	14
 Forms		
Form 1	Standard Procedure for Local Heating	22
Form 2	Standard Documentation Checklist for Local Heating	25

ASMENORMDOC.COM : Click to view the full PDF of ASME B31P 2017

FOREWORD

In 2011, the B31 Standards Committee for Pressure Piping determined that more consistency was needed between the B31 Code Sections regarding preheat and postweld heat treatment (PWHT) rules. The B31 Fabrication & Examination Technical Committee decided that a B31 Standard covering these rules would be the best way to provide this consistency; a proposal was developed, which was accepted by the B31 Standards Committee and the BPTCS.

This Standard is intended to provide requirements for preheating and PWHT when mandated by the applicable Code Section or by the engineering design being used. While the Code Sections provide only preheat and PWHT rules for ferrous materials, this Standard may provide expanded rules and alternatives for a wider variety of materials, although all materials that may be possible to use may not be covered.

Under direction of ASME Standards and Certification, both U.S. Customary and SI units are provided.

Following approval by the B31 Committee and ASME, and after public review, ASME B31P-2017 was approved by the American National Standards Institute on November 15, 2017.

ASME B31 COMMITTEE

Code for Pressure Piping

(The following is the roster of the Committee at the time of approval of this Standard.)

STANDARDS COMMITTEE OFFICERS

J. Meyer, *Chair*
J. Frey, *Vice Chair*
A. Maslowski, *Secretary*

STANDARDS COMMITTEE PERSONNEL

R. Appleby , ExxonMobil Pipeline Co.	J. Meyer , Louis Perry Group
C. Becht IV , Becht Engineering Co.	T. Monday , Team Industries, Inc.
K. Bodenhamer , TRC Pipeline Services	M. Nayyar , NICE
R. Bojarczuk	G. R. Petru , Acapella Engineering Services, LLC
M. R. Braz , MRBraz & Associates, PLLC	D. Rahoi , CCM 2000
J. Chin , TransCanada Pipeline U.S.	R. Reamey , Turner Industries Group, LLC
D. Christian , Victaulic	M. Rosenfeld , Kiefner/Applus — RTD
P. Deubler , Fronek Power Systems, LLC	J. Schmitz , Southwest Gas Corp.
C. Eskridge, Jr. , Jacobs Engineering	S. Sinha , Lucius Pitkin, Inc.
D. J. Fetzner , BP Exploration Alaska, Inc.	W. Sperko , Sperko Engineering Services, Inc.
P. Flenner , Flenner Engineering Services	J. Swezy, Jr. , Boiler Code Tech, LLC
J. Frey , Joe W. Frey Engineering Services, LLC	F. Tatar , FM Global
D. Frikken , Becht Engineering Co.	K. Vilminot , Black & Veatch
R. Grichuk , Fluor Enterprises, Inc.	G. Antaki , <i>Ex-Officio Member</i> , Becht Engineering Co., Inc.
R. Haupt , Pressure Piping Engineering Associates, Inc.	L. Hayden, Jr. , <i>Ex-Officio Member</i> , Consultant
G. Jolly , Samshin Limited	C. Kolovich , <i>Ex-Officio Member</i> , Kiefner
K. Kaplan , Consultant	A. Livingston , <i>Ex-Officio Member</i> , Kinder Morgan
A. Maslowski , The American Society of Mechanical Engineers	J. Willis , <i>Ex-Officio Member</i> , Page Southerland Page, Inc.
W. Mauro , American Electric Power	

B31 FABRICATION AND EXAMINATION COMMITTEE

J. Swezy, Jr. , <i>Chair</i> , Boiler Code Tech, LLC	S. Gingrich , AECOM
U. D'Urso , <i>Secretary</i> , The American Society of Mechanical Engineers	J. Hainsworth , WR Metallurgical
D. Bingham , Los Alamos National Labs	T. Monday , Team Industries, Inc.
R. Campbell , Bechtel	A. D. Nalbandian , Thielsch Engineering, Inc.
R. D. Couch , Electric Power Research Institute	R. Silvia , Process Engineers & Constructors, Inc.
R. J. Ferguson , Metallurgist	W. Sperko , Sperko Engineering Services, Inc.
P. Flenner , Flenner Engineering Services	K. Wu , Stellar Energy Systems
J. Frey , Joe W. Frey Engineering Services, LLC	

B31 MATERIALS TECHNICAL COMMITTEE

P. Deubler , <i>Chair</i> , Fronek Power Systems, LLC	C. Henley , Kiewit Engineering Group, Inc.
C. Eskridge, Jr. , <i>Vice Chair</i> , Jacobs Engineering	G. Jolly , Samshin Limited
C. O'Brien , <i>Secretary</i> , The American Society of Mechanical Engineers	C. Melo , TechnipFMC
B. Bounds , Bechtel Corp.	M. Nayyar , NICE
W. Collins , WPC Sol, LLC	D. Rahoi , CCM 2000
R. Grichuk , Fluor Enterprises, Inc.	R. Schmidt , Canadoil
J. Gundlach , Michigan Seamless Tube and Pipe	J. L. Smith , Consultant
A. Allah Hassan , PGESCO	Z. Djilali , Sonatrach
L. Henderson, Jr. , Chiyoda International Corp.	

B31 MECHANICAL DESIGN TECHNICAL COMMITTEE

G. Antaki, *Chair*, Becht Engineering Co., Inc.
J. Meyer, *Vice Chair*, Louis Perry Group
U. D'Urso, *Secretary*, The American Society of Mechanical Engineers
D. Arnett, Fluor
C. Becht IV, Becht Engineering Co.
R. Bethea, Huntington Ingalls Industries — Newport News Shipbuilding
N. Consumo, Sr.
J. P. Ellenberger
M. Engelkemier, Cargill
D. J. Fetzner, BP Exploration Alaska, Inc.
D. Fraser, NASA Ames Research Center
J. A. Graziano, Consultant

J. Hart, SSD, Inc.
R. Haupt, Pressure Piping Engineering Associates, Inc.
B. Holbrook
R. Leishear, Leishear Engineering, LLC
G. Mayers, Alion Science & Technology
T. McCawley, TQM Engineering, PC
J. Minichiello, Bechtel National, Inc.
P. Moore, Burns & McDonnell
A. Paulin, Paulin Research Group
R. Robledo, KBR
M. Rosenfeld, Kiefner/Applus — RTD
T. Sato, Japan Power Engineering and Inspection Corp.
M. Stewart, AECOM

TECHNICAL CONTRIBUTORS

D. Frikken, Becht Engineering Co.
I. Hadley, TWI Ltd.

C. Zimpel, BendTec, Inc.

CORRESPONDENCE WITH THE B31 COMMITTEE

General. ASME Standards are developed and maintained with the intent to represent the consensus of concerned interests. As such, users of this Standard may interact with the Committee by requesting interpretations, proposing revisions or a case, and attending Committee meetings. Correspondence should be addressed to:

Secretary, B31 Standards Committee
The American Society of Mechanical Engineers
Two Park Avenue
New York, NY 10016-5990
<http://go.asme.org/Inquiry>

Proposing Revisions. Revisions are made periodically to the Standard to incorporate changes that appear necessary or desirable, as demonstrated by the experience gained from the application of the Standard. Approved revisions will be published periodically.

The Committee welcomes proposals for revisions to this Standard. Such proposals should be as specific as possible, citing the paragraph number(s), the proposed wording, and a detailed description of the reasons for the proposal, including any pertinent documentation.

Proposing a Case. Cases may be issued to provide alternative rules when justified, to permit early implementation of an approved revision when the need is urgent, or to provide rules not covered by existing provisions. Cases are effective immediately upon ASME approval and shall be posted on the ASME Committee web page.

Requests for Cases shall provide a Statement of Need and Background Information. The request should identify the Standard and the paragraph, figure, or table number(s), and be written as a Question and Reply in the same format as existing Cases. Requests for Cases should also indicate the applicable edition(s) of the Standard to which the proposed Case applies.

Interpretations. Upon request, the B31 Standards Committee will render an interpretation of any requirement of the Standard. Interpretations can only be rendered in response to a written request sent to the Secretary of the B31 Standards Committee.

Requests for interpretation should preferably be submitted through the online Interpretation Submittal Form. The form is accessible at <http://go.asme.org/InterpretationRequest>. Upon submittal of the form, the Inquirer will receive an automatic e-mail confirming receipt.

If the Inquirer is unable to use the online form, he/she may mail the request to the Secretary of the B31 Standards Committee at the above address. The request for an interpretation should be clear and unambiguous. It is further recommended that the Inquirer submit his/her request in the following format:

Subject:	Cite the applicable paragraph number(s) and the topic of the inquiry in one or two words.
Edition:	Cite the applicable edition of the Standard for which the interpretation is being requested.
Question:	Phrase the question as a request for an interpretation of a specific requirement suitable for general understanding and use, not as a request for an approval of a proprietary design or situation. Please provide a condensed and precise question, composed in such a way that a "yes" or "no" reply is acceptable.
Proposed Reply(ies):	Provide a proposed reply(ies) in the form of "Yes" or "No," with explanation as needed. If entering replies to more than one question, please number the questions and replies.
Background Information:	Provide the Committee with any background information that will assist the Committee in understanding the inquiry. The Inquirer may also include any plans or drawings that are necessary to explain the question; however, they should not contain proprietary names or information.

Requests that are not in the format described above may be rewritten in the appropriate format by the Committee prior to being answered, which may inadvertently change the intent of the original request.

Moreover, ASME does not act as a consultant for specific engineering problems or for the general application or understanding of the Standard requirements. If, based on the inquiry information submitted, it is the opinion of the Committee that the Inquirer should seek assistance, the inquiry will be returned with the recommendation that such assistance be obtained.

ASME procedures provide for reconsideration of any interpretation when or if additional information that might affect an interpretation is available. Further, persons aggrieved by an interpretation may appeal to the cognizant ASME Committee or Subcommittee. ASME does not “approve,” “certify,” “rate,” or “endorse” any item, construction, proprietary device, or activity.

Attending Committee Meetings. The B31 Standards Committee regularly holds meetings and/or telephone conferences that are open to the public. Persons wishing to attend any meeting and/or telephone conference should contact the Secretary of the B31 Standards Committee.

ASMENORMDOC.COM : Click to view the full PDF of ASME B31P 2011

INTENTIONALLY LEFT BLANK

ASMENORMDOC.COM : Click to view the full PDF of ASME B31P 2017

STANDARD HEAT TREATMENTS FOR FABRICATION PROCESSES

1 INTRODUCTION

This Standard provides requirements for heat treatment of piping assemblies that meet the requirements of ASME B31 Code Sections. These requirements apply to

- (a) preheating
- (b) postweld heat treatment (PWHT)
- (c) postforming heat treatment (PFHT) required by the ASME B31 Code Sections for other fabrication processes, including forming processes such as bending

(d) heat treatments required by contract specifications

The heat treatments addressed in this Standard include weld preheating, PWHT, PFHT, and heat treatment in order to enhance material properties resulting from fabrication. Weld preheating is generally required on hardenable steels in order to reduce local hardness or to reduce the occurrence of hydrogen cracking. Preheat is typically required based on both hardenability (as indicated by the P-Number) and thickness at the weld. A minimum temperature for all materials prior to initiating a weld is expected to be needed to reduce the possibility of condensation. It should be noted that weld preheat is not usually considered a heat treatment, but it is a requirement of the ASME B31 Code Sections.

PWHT is generally required on hardenable steels in order to temper any hardened areas or to reduce residual stress in the weldment. PFHT may be used to address reduction of the properties within the bend after hot bending or to address the effects of strain after cold bending (the additional strain may cause a degradation of creep rupture properties when the operation is at high temperatures). In some cases of PWHT, PFHT, or material heat treatments, non-standard heat treatment may be required by the contract specification, e.g., an austenitizing heat treatment or a solution heat treatment.

This Standard is intended to provide consistent code heat treatment rules. It may be incorporated by reference in a code, or it can become a basis for code or contract requirements.

Appendices provide more-specific controls that may be needed or desired for specific applications. These specific controls are not mandatory unless specified.

Appendices are also included that outline alternative methods to exempt PWHT of welds when PWHT is difficult or impossible. The alternatives are required to be addressed within Welding Procedure Specifications (WPS) qualified in accordance with ASME Boiler and Pressure Vessel Code (BPVC), Section IX.

The requirements for the heat treatments done in accordance with material or product specifications are not addressed within this Standard. Such heat treatments are governed by those specifications.

2 GLOSSARY

creep strength enhanced ferritic (CSEF) steel: steel in which the microstructure, consisting of lower transformation products, e.g., martensite or bainite, is stabilized by controlled precipitation of temper-resistant carbides, carbonitrides, and/or nitrides.

heat treatments:

annealing, full: heating a metal to a temperature above the transformation temperature range and holding it above that range for a proper period of time, followed by cooling to below that range.

austenitizing: heat treatment where a partial or complete phase transformation to austenite occurs.

normalizing: a process in which a ferrous metal is heated to a suitable temperature above the transformation range and is subsequently cooled in still air at room temperature.

quenching: a process in which a ferrous metal is heated to a suitable temperature above the transformation range and is subsequently rapidly cooled in a selected quenching medium.

tempering: reheating a hardened metal to a temperature range below the transformation range.

interpass temperature: the highest temperature in the weld joint immediately prior to welding, or in the case of multiple pass welds, the highest temperature in the area of the previously deposited weld metal, immediately before the next pass is started.

postforming heat treatment (PFHT): any heat treatment subsequent to a bending or forming operation.

postweld heat treatment (PWHT): any heat treatment subsequent to welding.

postweld hydrogen bakeout: raising the temperature of a completed or partially completed weld for the purpose of allowing hydrogen to diffuse out of the weld or heat-affected zone (HAZ).

preheat: the heat applied to base metal immediately prior to a welding or cutting operation.

residual stress: stress that occurs in a weldment after all external loads have been removed.

3 TEMPERATURE MEASUREMENT

3.1 Measurement Method

3.1.1 Preheat. The preheat temperature shall be measured by use of thermocouples, pyrometers, temperature indication crayons, or other suitable temperature-measurement devices, to ensure that the required

preheat temperature is obtained prior to, and maintained during, the welding operation in the area to be welded immediately prior to welding.

3.1.2 Interpass Temperature. If required, the maximum interpass temperature shall be measured using devices allowed for preheat in [para. 3.1.1](#).

3.1.3 PWHT or Other Heat Treatments. The temperature shall be measured using thermocouples attached directly to the surface to ensure the temperature is uniform and controlled within the required limits. Noncontact temperature-measuring devices shall not be used.

3.1.4 Protection. If thermocouples are attached using methods other than the capacitor discharge welding process, the thermocouple site shall be protected from the direct heat of the heat source.

3.2 Attachment of Thermocouples

3.2.1 Recommendations for thermocouples are given in [Nonmandatory Appendix A](#).

3.2.2 Low-energy capacitor discharge welding may be used for the direct attachment of thermocouples without requiring preheat greater than 50°F (10°C) or subsequent PWHT (unless required for the weld joint), provided the following requirements are met:

(a) A Welding Procedure Specification (WPS) is prepared, describing the low-energy capacitor discharge welding equipment, the material to be welded on, and the technique of application. Qualification of this WPS is not required.

(b) The energy output of the low-energy capacitor discharge welding process is limited to 125 W-sec.

(c) Permanent thermocouple attachments or the surface from which temporary attachments are removed shall require visual examination but are exempt from further examination in accordance with code requirements.

4 TEMPERATURE CONTROL

4.1 Control of Heat Treatment Temperature

4.1.1 Minimum Requirements for Preheat. Minimum requirements are as follows:

(a) The base metal temperature for the parts to be welded shall be at or above the minimum temperature specified in all directions from the point of welding for a distance of the larger of 3 in. (75 mm) or 1.5 times the nominal material thickness (as defined in [para. 6.4.3](#)). For small-diameter piping less than 1½ in. (38 mm) outside diameter, the preheat distance from the weld may be reduced to the diameter of the piping in all directions or 1 in. (25 mm), whichever is greater. The base metal temperature for tack welds shall be at

or above the specified minimum temperature for a distance not less than 1 in. (25 mm) in all directions from the point of welding.

(b) Preheat above ambient temperature may be applied using flame, electric resistance, induction, quartz lamp, or infrared heating. If flame heating is used, the application shall use a dispersive method and, if manually applied, the temperature shall be continuously monitored to prevent excessive temperatures being reached.

(c) If methods are employed that utilize heating adjacent to the preheat area, allowing the heat to conduct along the part to the preheat area, the temperature of the part in the approximate center of the heated area shall also be monitored.

4.1.2 Minimum Requirements for Furnace Heat Treatment. Minimum requirements are as follows:

(a) Furnace heat treatment should be used when practical.

(b) An assembly may be heat treated in more than one heat in a furnace, provided there is at least a 12 in. (300 mm) overlap of the heated sections and the portion of the assembly outside the furnace is shielded so that the temperature gradient is not harmful. This method may not be used for austenitizing heat treatments on ferritic steels except for P-No. 1 carbon steels.

(c) Direct impingement of flame on the assembly is prohibited.

(d) The furnace shall be surveyed and calibrated such that the PWHT can be controlled within the required temperature range.

(e) Thermocouples shall be placed directly on components to be heat treated and shall be located on the thinnest and the thickest component(s) within the furnace. The placement of the thermocouples shall incorporate the high- and low-temperature locations within the furnace.

4.1.3 Minimum Requirements for Local Heat Treatment. Minimum requirements are as follows:

(a) PWHT may be performed locally by heating a circumferential band around the entire component, with the weld located in the approximate center of the band. The width of the band (soak band) heated to the specified temperature range shall be at least 3 times the nominal material thickness at the weld of the thickest part being joined. For nozzle and attachment welds, the width of the band heated to the specified temperature range shall extend beyond the nozzle weld, the reinforcement weld, or the attachment weld on each side at least 2 times the run-pipe nominal thickness and shall extend completely around the run pipe. Guidance for the placement of thermocouples on circumferential butt welds is provided in [Nonmandatory Appendix B](#). Special consideration shall be given to the placement of thermocouples when heating welds adjacent to large heat sinks, e.g.,

Table 5.1-1 Preheat Temperature

Base Metal P-Number [Note (1)]	Base Metal Group	Greater Nominal Material Thickness		Additional Limits	Required Minimum Temperature	
		in.	mm		°F	°C
1	Carbon steel	≤1	≤25	None	50	10
		>1	>25	%C ≤ 0.30 [Note (2)]	50	10
		>1	>25	%C > 0.30 [Note (2)]	200	95
3	Alloy steel Cr ≤ 1/2%	≤1/2	≤13	SMTS ≤ 65 ksi (450 MPa)	50	10
		>1/2	>13	SMTS ≤ 65 ksi (450 MPa)	200	95
		All	All	SMTS > 65 ksi (450 MPa)	200	95
4	Alloy steel 1/2% < Cr ≤ 2%	All	All	None	250	120
5A	Alloy steel	All	All	SMTS ≤ 60 ksi (414 MPa)	300	150
		All	All	SMTS > 60 ksi (414 MPa)	400	200
5B	Alloy steel	All	All	SMTS ≤ 60 ksi (414 MPa)	300	150
		All	All	SMTS > 60 ksi (414 MPa)	400	200
		>1/2	>13	%Cr > 6.0 [Note (2)]	400	200
6	Martensitic stainless steel	All	All	None	400 [Note (3)]	200 [Note (3)]
9A	Nickel alloy steel	All	All	None	250	120
9B	Nickel alloy steel	All	All	None	300	150
10I	27Cr steel	All	All	None	300 [Note (4)]	150 [Note (4)]
15E	9Cr-1Mo-V CSEF steel	All	All	None	400	200
All other materials				None	50	10

GENERAL NOTE: SMTS is an abbreviation for specified minimum tensile strength.

NOTES:

- (1) P-Numbers and Group Numbers are from ASME BPVC, Section IX, Table QW/QB-422.
- (2) Composition may be based on ladle or product analysis, or meeting specification limits.
- (3) Maximum interpass temperature 600°F (315°C).
- (4) Maintain interpass temperature between 300°F and 450°F (150°C and 230°C).

flanges, valves, or heavy fittings, or when joining parts of different thicknesses.

(b) No part of the materials subjected to the heat source shall be heated to a temperature exceeding the lower transformation temperature of the material. Particular care must be exercised when the applicable PWHT temperature is close to the material's lower transformation temperature, such as for CSEF steel materials or when materials of different P-Numbers are being joined. The requirements of Appendix B are mandatory for P-No. 15E materials.

(c) Local heat treating shall not be used for austenitizing heat treatments on ferritic steels except for P-No. 1 carbon steels.

4.2 Heating and Cooling Rates

4.2.1 Heating. Above 800°F (425°C), the rate of heating shall be not more than 600°F/hr (335°C/h) divided by the maximum material thickness in inches, but in no case more than 600°F/hr (335°C/h).

4.2.2 Cooling. Above 800°F (425°C), the rate of cooling shall be not more than 600°F/hr (335°C/h) divided by the maximum material thickness in inches, but in no case

more than 600°F/hr (335°C/h). (See Table 6.1.1-1 for special cooling rate requirements for certain materials.)

5 WELDING PREHEAT

5.1 Temperature

The minimum preheat temperature shall be as stated in Table 5.1-1 except as exempted in para. 3.2. Higher minimum preheat temperatures may be required by the WPS or as specified.

5.2 Different P-Number Materials

When welding two different P-Number materials, the minimum preheat temperature required shall be the temperature for the material with the higher required temperature, as shown in Table 5.1-1.

5.3 Interruption of Welding Preheat

After welding commences, the minimum preheat temperature shall be maintained until any required PWHT is performed on P-Nos. 3, 4, 5A, 5B, 6, and 15E materials, except when all of the following conditions are satisfied:

(a) A minimum of at least $\frac{3}{8}$ in. (10 mm) thickness of weld is deposited or 25% of the welding groove is filled, whichever is less (the weld shall be sufficiently supported to prevent overstressing the weld if the weldment is to be moved or otherwise loaded). Caution is advised that the surface geometry prior to cooling should be smooth and free of sharp discontinuities.

(b) For P-Nos. 3, 4, and 5A materials, the weld is allowed to cool slowly to room temperature.

(c) For P-Nos. 5B, 6, and 15E materials, the weld is subjected to an adequate postweld hydrogen bakeout with a controlled rate of cooling. The preheat temperature may be reduced to 200°F (95°C) (minimum) for the purpose of root examination without performing postweld hydrogen bakeout. A postweld hydrogen bakeout for P-Nos. 5B, 6, or 15E materials may be omitted when using low-hydrogen electrodes and filler metals classified by the filler metal specification with an optional supplemental diffusible-hydrogen designator of H4 or lower and suitably controlled by maintenance procedures to avoid contamination by hydrogen-producing sources. The surface of the base metal prepared for welding shall be free of contaminants.

(d) After cooling and before welding is resumed, visual examination of the weld shall be performed to assure that no visible cracks have formed.

(e) The joint shall be preheated before welding is resumed.

6 POSTWELD HEAT TREATMENT (PWHT)

6.1 Minimum PWHT Requirements

6.1.1 Temperature Range for PWHTs. A qualified welding procedure specification (WPS) in accordance with ASME BPVC, Section IX, shall be available before applying the detailed requirements and exemptions in these paragraphs. All welds in materials included in the P-Numbers listed in [Table 6.1.1-1](#) shall be given a PWHT within the temperature range specified, except as otherwise provided in [paras. 6.2](#) and [6.3](#), and in [Tables 6.1.1-2](#) and [6.1.1-3](#). (The range specified in [Table 6.1.1-1](#) may be modified by [Table 6.1.1-2](#) for the lower limit and [para. 6.2](#) for the upper limit.) The materials in [Table 6.1.1-1](#) are listed in accordance with the material P-Numbers and Group Numbers of ASME BPVC, Section IX, Table QW/QB-422. Welds on materials not included in [Table 6.1.1-1](#) shall be heat treated in accordance with the WPS. Austenitizing PWHTs on ferritic materials may be performed in lieu of the heat treatments specified herein if required by the qualified WPS being followed.

6.1.2 PWHT for High-Cr Filler Metal Welds. Pressure-part welds and attachment welds using ferritic filler metals that have a specified chromium content of more than 3% shall receive a postweld heat treatment. The postweld heat treatment time and temperature range used

shall be that shown in [Table 6.1.1-1](#) for any base metal of similar composition.

6.1.3 Hardness. Hardness tests are not required to verify proper heat treatment unless otherwise specified in the engineering design.

6.2 Mandatory PWHT Requirements

Heat treatment may be accomplished by a suitable heating method that will provide the desired heating and cooling rates, the required metal temperature, temperature uniformity, and temperature control.

(a) The upper limit of the PWHT temperature range in [Table 6.1.1-1](#) is a recommended value that may be exceeded, provided the actual temperature does not exceed the lower transformation temperature of either material (see [Table 6.2-1](#)).

(b) When parts of two different P-Numbers are joined by welding, the postweld heat treatment shall be that specified for the material requiring the higher PWHT temperature. When a nonpressure part is welded to a pressure part and PWHT is required for either part, the maximum PWHT temperature shall not exceed the maximum temperature acceptable for the pressure-retaining part.

(c) Caution is necessary to preclude metallurgical damage to some materials or welds not intended or qualified to withstand the PWHT temperatures required. The use of material transition joint designs may be required.

(d) The PWHT may be specified even if not mandatory in accordance with [Table 6.1.1-1](#) or [Table 6.1.1-3](#).

6.3 Exemptions to Mandatory PWHT Requirements

6.3.1 Exemptions. For the following welds, postweld heat treatment is not required unless required by the contract specification or the qualified WPS:

(a) welds in nonferrous materials except as required in [Table 6.1.1-1](#)

(b) welds exempted in [Tables 6.1.1-1](#) and [6.1.1-3](#)

(c) welds subject to temperatures during subsequent fabrication above the lower transformation temperature, provided the WPS has been qualified with PWHT at the temperature range to be reached

(d) thermocouple attachments made by low-energy capacitor discharge welding as exempted in [para. 3.2](#)

6.3.2 Chemical Composition. The postweld heat treatment exemptions of [Tables 6.1.1-1](#) and [6.1.1-3](#) may be based on the actual chemical composition as determined by a ladle or product analysis in accordance with the material specification, in lieu of the specified or maximum specified chemical composition limits. Alternatively, the actual chemical composition may be determined by analysis of the material.

Table 6.1.1-1 Postweld Heat Treatment

P-Number, Group Number (ASME BPVC Section IX, Table QW/QB-422)	Holding Temperature Range, °F (°C) [Notes (1) and (2)]	Minimum Holding Time at Temperature for Control Thickness [Note (3)]	
		Up to and Including 2 in. (50 mm)	Over 2 in. (50 mm)
P-No. 1, Group Nos. 1–3	1,100 to 1,200 (595 to 650)	1 hr/in. (1 h/25 mm), 15 min minimum	2 hr plus 15 min for each additional inch (25 mm) over 2 in. (50 mm)
P-No. 3, Group Nos. 1 & 2	1,100 to 1,200 (595 to 650)		
P-No. 4, Group Nos. 1 & 2	1,200 to 1,300 (650 to 705)		
P-No. 5A, Group No. 1	1,250 to 1,400 (675 to 760)		
P-No. 5B, Group No. 1	1,250 to 1,400 (675 to 760)		
P-No. 6, Group Nos. 1–3	1,400 to 1,475 (760 to 800)		
P-No. 7, Group Nos. 1 & 2 [Note (4)]	1,350 to 1,425 (730 to 775)		
P-No. 8, Group Nos. 1–4	PWHT not required unless required by WPS		
P-No. 9A, Group No. 1	1,100 to 1,200 (595 to 650)		
P-No. 9B, Group No. 1	1,100 to 1,175 (595 to 630)		
P-No. 10H, Group No. 1	PWHT not required unless required by WPS. If done, see [Note (5)].		
P-No. 10I, Group No. 1 [Note (4)]	1,350 to 1,500 (730 to 815)	1 hr/in. (1 h/25 mm), 30 min minimum	1 hr/in. (1 h/25 mm) up to and including 5 in. (125 mm) plus 15 min for each additional inch (25 mm) over 5 in. (125 mm)
P-No. 15E, Group No. 1	1,300 to 1,425 (705 to 775) [Notes (6) and (7)]		
All other materials	PWHT as required by WPS	In accordance with WPS	In accordance with WPS

NOTES:

- (1) The exemptions for mandatory PWHT are defined in Table 6.1.1-3.
- (2) The holding temperature range is further defined in paras. 6.1.1 and 6.2.
- (3) The control thickness is defined in para. 6.4.1.
- (4) Cooling rate shall not be greater than 100°F (55°C) per hour in the range above 1,200°F (650°C), after which the cooling rate shall be sufficiently rapid to prevent embrittlement.
- (5) If heat treatment is performed after bending, forming, or welding, it shall be within the following temperature ranges for the specific alloy, followed by rapid cooling:
 - (a) UNS Nos. S31803 and S32205 — 1,870°F to 2,010°F (1 020°C to 1 100°C)
 - (b) UNS No. S32550 — 1,900°F to 2,050°F (1 040°C to 1 120°C)
 - (c) UNS No. S32750 — 1,880°F to 2,060°F (1 025°C to 1 125°C)
 - (d) all others — 1,800°F to 1,900°F (980°C to 1 040°C)
- (6) The minimum PWHT holding temperature may be 1,250°F (675°C) for nominal material thicknesses (see para. 6.4.3) up to and including ½ in. (13 mm).
- (7) The Ni + Mn content of the filler metal shall not exceed 1.2% unless specified, in which case the maximum temperature to be reached during PWHT shall be the A_1 (lower transformation or lower critical temperature) of the filler metal, as determined by analysis and calculation or by test, but not exceeding 1,470°F (800°C). If the 1,470°F (800°C) was not exceeded but the A_1 of the filler metal was exceeded, or if the composition of the filler metal is unknown, the weld must be removed and replaced. It shall then be rewelded with compliant filler metal and subjected to a compliant PWHT. If the 1,470°F (800°C) limit was exceeded, the weld and the entire area affected by the PWHT will be removed and, if reused, shall be renormalized and tempered prior to reinstallation.

Table 6.1.1-2 Alternate Postweld Heat Treatment Requirements for Carbon and Low-Alloy Steels, P-Nos. 1 and 3

Decrease in Specified Minimum Temperature, °F (°C)	Minimum Holding Time at Decreased Temperature, hr [Note (1)]
50 (30)	2
100 (55)	4
150 (85) [Note (2)]	10
200 (110) [Note (2)]	20

NOTES:

- (1) Times shown apply to thicknesses up to and including 1 in. (25 mm). Add 15 min/in. (15 min/25 mm) of thickness for control thicknesses over 1 in. (25 mm). See para. 6.4.
- (2) A decrease greater than 100°F (55°C) below the minimum specified temperature is allowable only for P-No. 1, Group Nos. 1 and 2 materials.

6.4 Definition of Thicknesses Governing PWHT

6.4.1 Control Thickness. *Control thickness* as used in Tables 6.1.1-1 and 6.1.1-3 is the lesser thickness of (a) or (b) as follows:

(a) the thickness of the weld (not including reinforcement)

(b) the thicker of the materials being joined at the weld or the thickness of the pressure-containing material if the weld is attaching a nonpressure-containing material to a pressure-containing material

6.4.2 Weld Thickness. *Weld thickness*, which is a factor in determining the control thickness, is defined as follows:

(a) groove welds (girth and longitudinal) — the thicker of the two abutting ends at the weld preparation, including machining of the inside or outside diameters

(b) fillet welds — the throat thickness of the weld

(c) partial-penetration welds — the depth of the weld groove preparation

(d) material-repair welds — the depth of the cavity to be repaired

(e) branch-connection welds — the weld thickness is the dimension that exists in a plane that intersects the longitudinal axes and is calculated as indicated for each detail using

$$t_c = \text{the smaller of } \frac{1}{4} \text{ in. (7 mm) or } 0.7t_{nb}$$

(1) for full-penetration branch-connection welds without a reinforcing pad or saddle

$$\text{weld thickness} = t_c + t_{nb} \text{ or } t_c + t_{nh}$$

where t_{nb} or t_{nh} is chosen based on the component that receives the full penetration weld

(2) for full-penetration branch-connection welds with a reinforcing pad or saddle

$$\text{weld thickness} = t_{nr} + \text{the weld thickness calculated in (e)(1)}$$

(3) for partial penetration branch connection welds

$$\text{weld thickness} = t_c + \text{the depth of the partial-penetration weld preparation}$$

where

t_c = nominal throat of cover fillet welds on branch connections

t_{nb} = nominal thickness of a branch pipe

t_{nh} = nominal thickness of a header or a run pipe

t_{nr} = nominal thickness of added reinforcement

NOTE: Typical branch connection details are shown in Nonmandatory Appendix C.

6.4.3 Nominal Material Thickness. *Nominal material thickness* as used in Table 6.1.1-3 is the thicker of the pressure-retaining materials being joined at the weld. If the material thicknesses are measured to determine the actual material thickness, the measured material thickness(es) may be used to determine the PWHT hold-time requirements or exemptions for each joint on a case-by-case basis.

7 POSTFORMING AND MATERIAL HEAT TREATMENTS

This section covers postforming heat treatments (PFHT) and heat treatments intended to enhance the material microstructure.

7.1 PFHT

7.1.1 Hot Bending

7.1.1.1 Definition. *Hot bending* is a bending or forming process accomplished at a temperature above 1,300°F (705°C).

7.1.1.2 PFHT Requirements for Hot Bending and Forming. The applicable code or the design may require PFHT to recover material properties or to recover creep strength. Typically, the required heat treatment may involve normalizing and tempering or other heat treatment to recover the desired material condition.

7.1.2 Cold Bending

7.1.2.1 Definition. *Cold bending* is a bending or forming process accomplished at a temperature at or below 1,300°F (705°C).

7.1.2.2 PFHT Requirements for Cold Bending and Forming. The applicable code or the design may require PFHT to recover creep strength or to reduce residual stresses for components that have experienced cold strain. The required heat treatment may be a subcritical

Table 6.1.1-3 Exemptions to Mandatory Postweld Heat Treatment

P-Number, Group Number (ASME BPVC, Section IX, Table QW-422) [Note (1)]	Control Thickness, in. (mm) [Note (2)]	Type of Weld	Additional Limitations Required for Exemption From PWHT [Notes (3), (4), and (5)]
P-No. 1, Group Nos. 1-3	All	All	1. Preheat of 200°F (95°C) is applied prior to welding on any nominal material thickness > 1 in. (25 mm) 2. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
P-No. 3, Group Nos. 1 and 2	$\leq \frac{5}{8}$ in. (16 mm), except the thickness of a socket weld fitting or flange need not be considered	All	1. Preheat of 200°F (95°C) is applied prior to welding on any nominal material thickness > $\frac{1}{2}$ in. (13 mm) 2. Specified carbon content of the base materials $\leq 0.25\%$ 3. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
P-No. 4, Group No. 1	$\leq \frac{5}{8}$ in. (16 mm)	Groove	1. Mandatory preheat has been applied 2. Specified carbon content of the base materials $\leq 0.15\%$ 3. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
	$\leq \frac{5}{8}$ in. (16 mm), except the thickness of a socket weld fitting or flange need not be considered	Socket and fillet welds	1. Mandatory preheat has been applied 2. Throat thickness of the fillet weld or socket weld $\leq \frac{1}{2}$ in. (13 mm) 3. Specified carbon content of the pipe material $\leq 0.15\%$ 4. Nominal material thickness of the pipe $\leq \frac{5}{8}$ in. (16 mm) 5. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
	$\leq \frac{5}{8}$ in. (16 mm)	Seal welds and non-load-carrying attachments [Note (7)]	1. Mandatory preheat has been applied 2. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
	$\leq \frac{5}{8}$ in. (16 mm)	Groove	1. Mandatory preheat has been applied 2. Specified carbon content of the base materials $\leq 0.15\%$ 3. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
	$\leq \frac{5}{8}$ in. (16 mm), except the thickness of a socket weld fitting or flange need not be considered	Socket and fillet welds	1. Mandatory preheat has been applied 2. Throat thickness of the fillet weld or socket weld $\leq \frac{1}{2}$ in. (13 mm) 3. Specified carbon content of the pipe material $\leq 0.15\%$ 4. Nominal material thickness of the pipe $\leq \frac{5}{8}$ in. (16 mm) 5. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
	$\leq \frac{5}{8}$ in. (16 mm)	Seal welds and non-load-carrying attachments [Note (7)]	1. Mandatory preheat has been applied 2. Multiple layer welds are used when nominal material thickness > $\frac{3}{16}$ in. (5 mm) [Note (6)]
P-No. 5B, Group No. 1	No exemptions from PWHT		
P-No. 6, Group Nos. 1-3	All	All	1. Specified carbon content of the base materials $\leq 0.08\%$ 2. Nominal material thickness $\leq \frac{3}{8}$ in. (10 mm) 3. Weld filler metal is A-No. 8, A-No. 9, or F-No. 43 composition [Note (8)]
P-No. 7, Group No. 1	All	All	1. Specified carbon content of the base materials $\leq 0.08\%$ 2. Nominal material thickness $\leq \frac{3}{8}$ in. (10 mm) 3. Weld filler metal is A-No. 8, A-No. 9, or F-No. 43 composition [Note (8)]
P-No. 7, Group No. 2	No exemptions from PWHT		

Table 6.1.1-3 Exemptions to Mandatory Postweld Heat Treatment (Cont'd)

P-Number, Group Number (ASME BPVC, Section IX, Table QW/QB-422) [Note (1)]	Control Thickness, in. (mm) [Note (2)]	Type of Weld	Additional Limitations Required for Exemption From PWHT [Notes (3), (4), and (5)]
P-No. 8, Group Nos. 1-4 All	All	All	PWHT neither required nor prohibited
P-No. 9A, Group No. 1 All	All	All	1. Specified carbon content of the pipe material $\leq 0.15\%$ 2. Nominal material thickness $\leq \frac{1}{2}$ in. (13 mm) 3. Mandatory preheat has been applied
P-No. 9B, Group No. 1 All	All	All	Nominal material thickness $\leq \frac{5}{8}$ in. (16 mm) and the WPS has been qualified using a material of equal or greater thickness than used in the production weld
P-No. 10H, Group No. 1 All	All	All	PWHT neither required nor prohibited
P-No. 10I, Group No. 1 All	All	All	PWHT neither required nor prohibited for nominal material thickness $\leq \frac{1}{2}$ in. (13 mm)
P-No. 15E	No exemptions from PWHT		

NOTES:

- (1) If differences with the P-Number listed in Nonmandatory Appendix A are found, the P-Number listed in ASME BPVC, Section IX, Table QW/QB-422 applies.
- (2) The control thickness is defined in para. 6.4.1.
- (3) The nominal material thickness is defined in para. 6.4.3.
- (4) No exemptions are permitted for PWHTs required by the WPS or as specified.
- (5) Additional exemptions for welds made in accordance with para. 3.2.2 may be taken for the materials addressed.
- (6) Single-layer or single-pass welds may be exempted from PWHT, provided the WPS has been qualified using single-pass welds with $\pm 10\%$ heat input and that all other conditions for exemption are met.
- (7) Non-load-carrying attachments are defined as items where no pressure loads or significant mechanical loads are transmitted through the attachment to the pipe or pressure-containing material.
- (8) A-Numbers and F-Numbers are found in ASME BPVC, Section IX, Tables QW-442 and QW-432, respectively.

Table 6.2-1 Approximate Lower Transformation Temperatures

Material	Approximate Lower Transformation Temperature, °F (°C)
Carbon steel (P-No. 1)	1,340 (725)
Carbon-molybdenum steel (P-No. 3)	1,350 (730)
1Cr-½Mo (P-No. 4)	1,375 (745)
1¼Cr-½Mo (P-No. 4)	1,430 (775)
2¼Cr-1Mo and 3Cr-1Mo (P-No. 5A)	1,480 (805)
5Cr-½Mo (P-No. 5B)	1,505 (820)
9Cr-1Mo (P-No. 5B)	1,475 (800)
9Cr-1Mo-V (P-No. 15E)	1,470 (800)

GENERAL NOTE: These values are intended for guidance only. The user may apply values obtained for the specific material in lieu of these values.

heat treatment in accordance with [Table 6.1.1-1](#), a stress-relieving heat treatment for austenitic materials, or a normalizing and tempering heat treatment as specified by the applicable code or the design.

7.2 Material Heat Treatment

A material heat treatment is not applicable when the heat treatment is accomplished as a requirement of a material specification. Heat treatment in accordance with this Standard may be specified when fabrication degrades the desired material properties.

8 ALTERNATIVES AND EXEMPTIONS TO PREHEAT AND PWHT REQUIREMENTS

Exemptions to the rules for preheat and PWHT in [sections 5](#) and [6](#) may be taken provided the specifying organization and the applicable regulatory authority agree. The WPS shall be qualified in accordance with ASME BPVC, Section IX for the alternative preheat or PWHT to be used. The following are examples of exemptions:

(a) requiring an austenitizing PWHT on ferritic materials or a stress relief on austenitic materials

(b) requiring PWHT when necessary to enhance corrosion resistance even if the PWHT is not required by this Standard

(c) allowing low-temperature preheat [not below 50°F (10°C)] when other methods to specifically control high hardness or the susceptibility to hydrogen cracking are exercised

(d) accepting temper bead welding alternatives to PWHT if qualified in accordance with the rules of ASME BPVC, Section IX, QW-290 and the requirements of [Nonmandatory Appendix D](#)

(e) accepting fracture mechanics analysis as an alternative to otherwise required PWHT if qualified in accordance with the rules of ASME BPVC, Section IX and the requirements of [Nonmandatory Appendix E](#)

NONMANDATORY APPENDIX A RECOMMENDATIONS FOR THE PROPER USE OF THERMOCOUPLES

A-1 THERMOCOUPLE TYPES AND USAGE

Thermocouples shall be selected based upon their maximum recommended temperature rating.

Type J, Iron-Constantan shall not be used above 1,400°F (760°C).

Type K, Chromel-Alumel shall not be used above 2,300°F (1 260°C).

A-2 PERMISSIBLE THERMOCOUPLE WIRE SIZE

The maximum thermocouple wire size shall not exceed 20 gage except when attached using the low-energy capacitor discharge method, where the maximum size shall be 22 gage. The minimum size shall be 24 gage.

A-3 LOCATION

Each wire shall be attached separately to the surface of the workpiece, with the wires in close proximity [approximately $\frac{1}{4}$ in. (6 mm)] to each other. Maximum separation of the wires shall be held to $\frac{1}{4}$ in. (6 mm).

A-4 ATTACHMENT

The recommended attachment of thermocouples is in accordance with [para. 3.2](#).

A-5 REMOVAL OF THERMOCOUPLES

During the removal stage, the location of each thermocouple should be adequately identified. Light filing or grinding followed by visual examination of the thermocouple attachment areas may be required. Care must always be exercised during filing or grinding to prevent removal of too much metal.

NONMANDATORY APPENDIX B

RECOMMENDATIONS FOR CONTROL OF NARROW TEMPERATURE RANGE HEAT TREATMENTS: LOCAL HEAT-TREATMENT METHODS

B-1 SCOPE

This Appendix describes the recommendations to be followed during the setup and application of local controlled PWHT when using electric resistance heating pads. The recommendations are required for P-No. 15E or other CSEF steel PWHTs [see [para. 4.1.3 \(b\)](#)]. They are strongly recommended for dissimilar material welds where multiple temperature ranges overlap, requiring control of narrow ranges.

B-2 INTRODUCTION

During the manufacture, fabrication, or repair of P-No. 15E piping components, it may be necessary to heat components before welding (preheating), between passes (interpass heating), or after welding (hydrogen bakeout or PWHT). Typically, heat treatments are required by design or the applicable codes. Heat treatments can degrade materials or weldments if not properly accomplished by experienced personnel using controlled heat-treatment processes. If possible, local PWHT should be avoided in longitudinal welds due to higher pressure stresses, particularly for welds in CSEF steels. Furnace normalizing and tempering may be required by design.

B-3 GLOSSARY AND NOMENCLATURE FOR LOCAL HEATING

B-3.1 Glossary

This paragraph defines the terms used in describing local circumferential band heating. See [Figures B-3.1-1](#) and [B-3.1-2](#). Minimum requirements for these regions are presented in [para. B-4](#).

axial temperature gradient: the change in temperature along the length of the component. This is usually stated as a maximum temperature difference between two points located a specified distance apart.

component orientation: for the purposes of this Standard, cylindrical components or PWHT in the horizontal position shall mean that the longitudinal axis of the main component lies in the horizontal position, and in the

vertical position shall mean that the longitudinal axis of the main component lies in the vertical position.

control thermocouple: single temperature-measuring device that is located within the control zone in order to control the temperature of that control zone.

control zone: a grouping of one or more electrical heating pads that are controlled electrically based upon input from a single temperature-measuring device (typically a thermocouple). One or more zones may be present in the circumferential and/or axial directions.

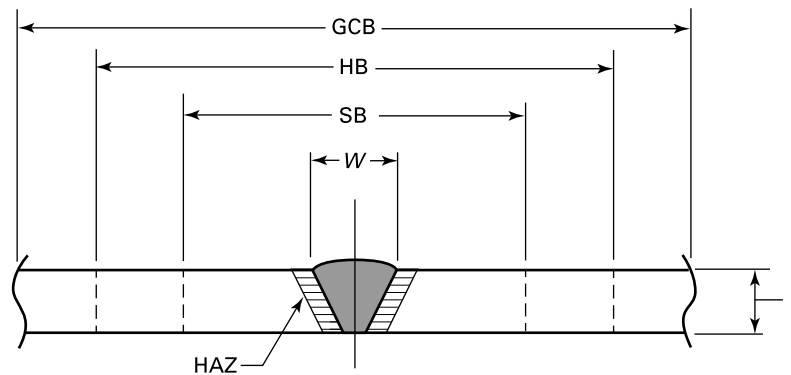
gradient control band (GCB): surface area over which insulation and/or supplementary heat source(s) may be placed. The gradient control band encompasses the soak band, the heated band, and sufficient adjacent base metal to ensure that harmful temperature gradients are not generated within the heated band.

gradient control heaters: under certain circumstances, extra heaters known as gradient control heaters or blocking heaters are installed adjacent to the heated band, to add additional heat to control thermal temperature gradients, or to provide thermal biasing to counter increased thermal mass or to counter a vertical bias in the temperature distribution in the heated band during PWHT in the vertical position.

heated band (HB): surface area over which the heat is applied to achieve the required temperature in the soak band. The heated band consists of the soak band width on the outside surface of the component, plus any adjacent base metal necessary to both control the temperature and achieve an acceptable temperature on the inside of the pipe or tube.

monitoring thermocouple: temperature-measuring device used to measure the temperature at the position where it is located.

soak band (SB): through-thickness volume of metal that is required to be heated to within the postweld heat treatment temperature range. As a minimum, it shall consist of the weld metal, the HAZ, and a portion of the base metal adjacent to and on each side of the weld being heated.

Figure B-3.1-1 Definition of Terms for Local Circumferential Band Heating of Pipe Weld

through-thickness temperature gradient: the difference between the temperature on the outside of the weld or component and the temperature on the inside of that same component, on the same radial line, and in the same axial plane.

B-3.2 Nomenclature

HAZ = heat-affected zone
 t = nominal thickness of piping, branch connection, nozzle neck, or attachment
 W = widest width of butt or attachment weld

B-4 LOCAL CIRCUMFERENTIAL BAND HEATING

Local heating of parts or components shall be accomplished by heating circumferential bands. Since local heating of piping is typically from the outside, when designing heat treatment procedures, radial (through-thickness) temperature gradients shall be considered.

B-4.1 Soak Band

The soak-band width for PWHT shall as a minimum be equal to the following. The thickness, t , is typically the nominal pipe wall thickness but measured thicknesses may be used.

(a) The minimum soak-band width requirement for PWHT shall be at least $3t$ with the weld at the centerline.

(b) For piping less than or equal to NPS 4 (DN 100), the soak band shall be $1.5t$ on each side of the weld at its greatest width.

(c) For piping greater than NPS 4 (DN 100) but less than or equal to NPS 8 (DN 200), the soak band shall be $6t$ on each side of the weld at its greatest width.

(d) For piping greater than NPS 8 (DN 200), the soak band shall be $10t$ on each side of the weld at its greatest width.

B-4.2 Heated Band

The minimum requirement for hydrogen bakeout heating shall be the lesser of t or 2 in. (50 mm) on each side of the weld at its greatest width.

The minimum requirement for the heated-band width shall be the soak-band width plus 2 in. (50 mm).

B-4.3 Gradient Control Band

The primary function of this band is to control the axial temperature gradient at the edges of the heated band. It also serves to minimize heat losses in the heated band. The width of the insulated area directly affects the axial temperature gradient. The insulated width may also need to be increased for personnel protection.

The gradient-control-band width shall as a minimum be equal to or greater than the heated-band width plus $4t$ on each side of the weld.

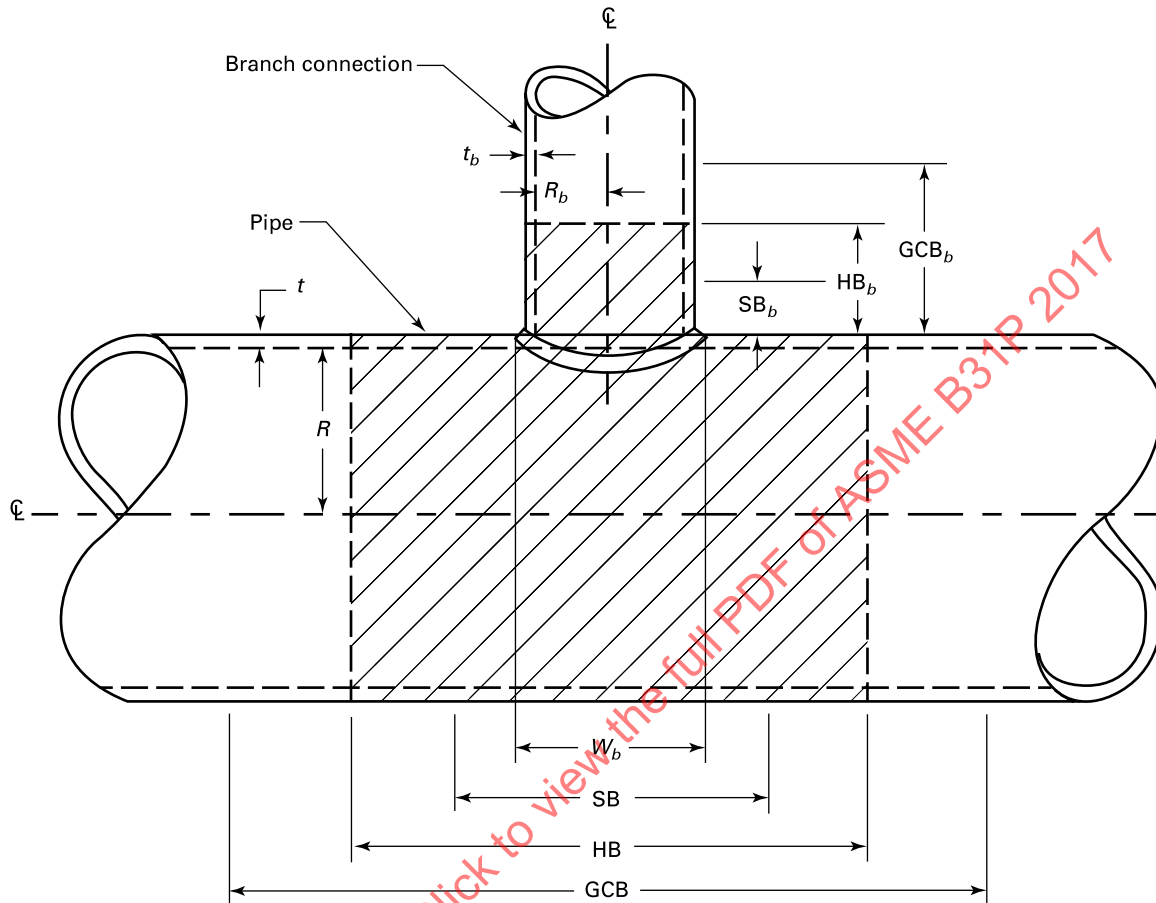
If the pipe-wall thickness changes, attachments are present within the gradient control band, or the pipe is being welded to flanges or valves, the use of supplemental heat source(s) within the gradient control band may be required.

B-4.4 Axial Temperature Gradient

The axial temperature distribution plays an important role in limiting induced stresses during PWHT. The temperature gradient shall be controlled such as to be reasonably uniform around the component.

During the heating, holding time, and cooling, the maximum axial temperature gradient for PWHT shall be limited such that the temperature at the edge of the heated band shall be no less than one-half the temperature at the edge of the soak band.

Figure B-3.1-2 Definition of Terms for Local Circumferential Band Heating of Branch Connection to Pipe Attachment Weld



LEGEND:

GCB, GCB_b = gradient control band (minimum width of insulation and/or gradient heat source)

HB, HB_b = heated band (width of heat source), shown as shaded area

R, R_b = inside radius of pipe or branch connection

SB = soak band on pipe (width of the volume of the material where the holding temperature equals or exceeds the minimum and equals or is below the maximum required. The minimum width is typically specified as W_b plus a multiple of t on each side of the weld attaching the branch connection.)

SB_b = soak band on branch connection. The minimum width is typically specified as a multiple of t_b beyond the widest width of the weld attaching the branch connection.

t , t_b = nominal thickness of pipe or branch connection

W_b = widest width of weld attaching the branch connection to the pipe

Table B-5.1-1 Requirements for Control Zones

Equivalent Pipe Size	Minimum Required Number of Circumferential Control Zones and Control Thermocouple Locations
Less than NPS 6 (DN 150)	One control zone, with the control thermocouple at 12 o'clock
NPS 6 (DN 150) up to and including NPS 12 (DN 300)	Two control zones, with control thermocouples at 12 o'clock and 6 o'clock
NPS 14 (DN 350) up to and including NPS 30 (DN 750)	Four control zones, with control thermocouples at 12 o'clock, 3 o'clock, 6 o'clock, and 9 o'clock
Over NPS 30 (DN 750)	Number of control zones and control thermocouples as required by actual heater configuration, circumferential spacing of heaters, and control bands, with at least one control thermocouple at 12 o'clock

B-5 DESIGN OF THE HEATING PROCESS

The design shall be as follows:

(a) Choice of the sizes, the number, and the electrical configuration of electric heating pads shall be based upon the geometrical configuration of the parts, the soak-band area, and the heated-band areas.

(b) All heating pads used in a single heat treatment shall be manufactured from the same materials and of the same watt density.

(c) Prior to installation, each heater shall be inspected for broken ceramic beads and frayed heater wires. If found and judged to be detrimental to the process, the heaters shall be replaced.

(d) Heating pads shall be symmetrically located on either side of the weld preparation.

(e) Each control zone shall have at least one control thermocouple installed.

(f) In the case of horizontally oriented pipe and tube, a control thermocouple shall be installed at the 12 o'clock position.

(g) In the case of vertically oriented pipe and tube, at least one monitoring thermocouple shall be installed at the upper edge of the uppermost heating pad.

(h) One control or monitoring thermocouple shall be installed under each heater.

B-5.1 Postweld Heat Treatment

PWHT shall be as follows:

(a) The heating pads shall be installed to minimize gaps between the heaters. The gaps between the heaters shall not be greater than $\frac{3}{8}$ in. (10 mm) when the nominal wall thickness of the pipe is less than or equal to 1 in. (25 mm). The gaps between the heaters shall not be greater than one-third the wall thickness when the nominal wall thickness of the pipe exceeds 1 in. (25 mm). Where this is not possible, a monitoring thermocouple shall be placed in the center of all gaps that exceed this limit. The temperature shall not be less than the minimum soak band temperature within the gap.

(b) Overlapping of heaters is not allowed.

(c) Heater tails shall not be allowed to cross any other pad or heater tail.

(d) Heater tails shall be insulated from the pipe and shall be brought out through the insulation as close to the edge of the heater as possible.

(e) Control zones for horizontal piping shall as a minimum be in accordance with Table B-5.1-1.

(f) The number of control zones for vertical piping shall be in accordance with Table B-5.1-1. Separate control zones, above and below the weld, are required when more than one zone is required.

(g) Monitoring thermocouples shall also be installed at the outer edges of the soak band and at the outer edges of the heated band.

(h) The control zones for PWHT of welds joining piping to a thicker component or thicker pipe may require separate control zones for the thicker and thinner components. In such instances, additional monitoring thermocouples are recommended to ensure that the required temperatures are achieved on both the thinner and heavier wall thickness components.

B-5.2 Examples of Thermocouple Locations

Figures have been provided to show examples of the thermocouple locations for common local circumferential band PWHT applications. In some instances, both monitoring and control thermocouples are shown. Figures B-5.2-1 through B-5.2-3 provide required monitoring and control thermocouple locations for PWHT of butt welds in horizontally oriented piping with one, two, and four zones of control. Figure B-5.2-4 provides required monitoring thermocouple locations for PWHT of a weld attaching a branch connection to pipe. Control thermocouples shall be attached as required by the control-zone layout.

B-5.3 Special Considerations

Due to natural internal convection heat flow, the upper side of the soak or heated zones may be considerably hotter than the lower side. To help avoid exceeding the maximum allowed temperature, the following shall be considered in addition to the requirements in the Standard:

(a) *Horizontal Piping.* One control thermocouple shall always be installed at the 12 o'clock position for horizontal piping.

Figure B-5.2-1 Location of Thermocouples (Monitoring and Control) for Pipe Sizes Less Than NPS 6 (150 DN) and One Control Zone

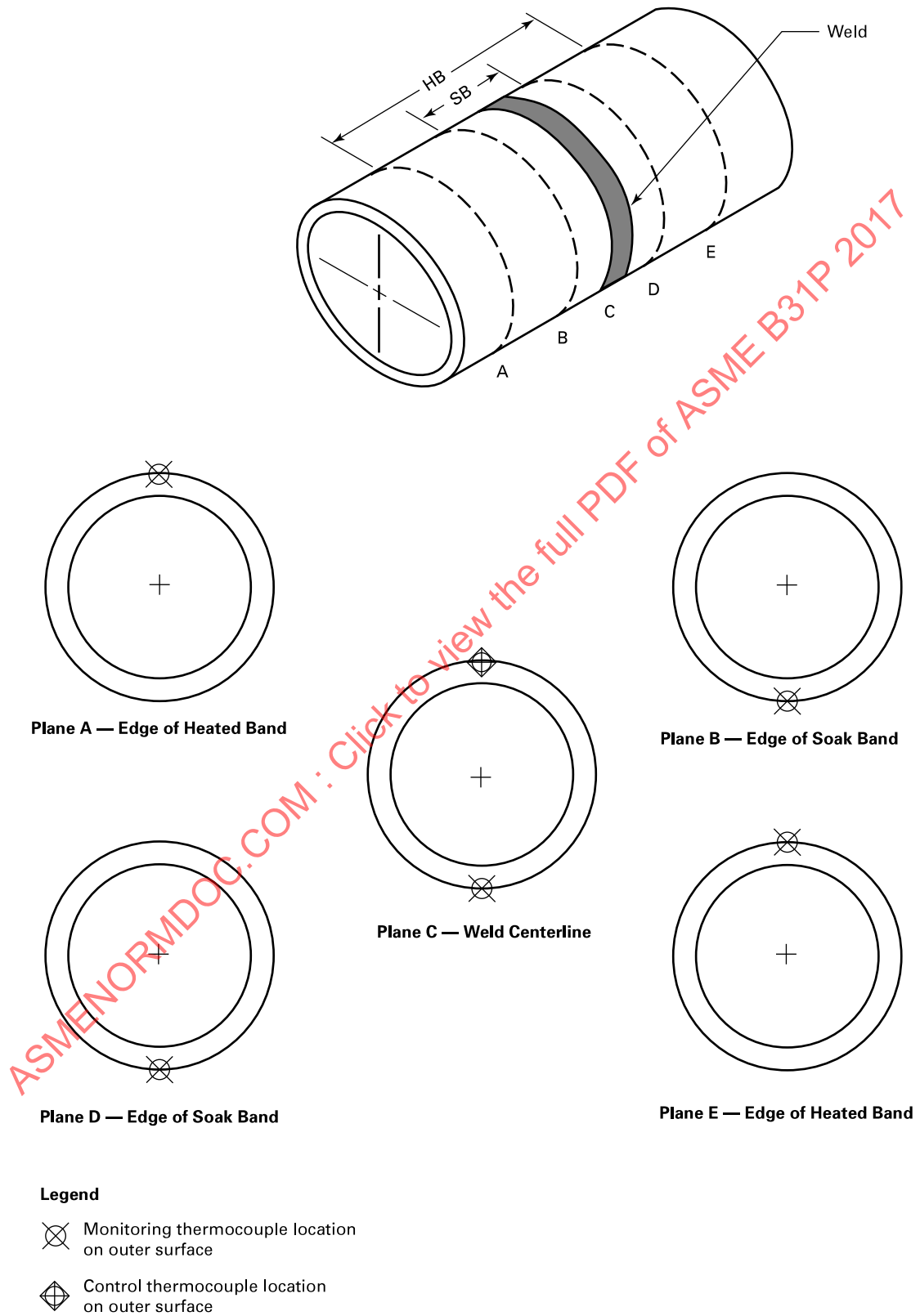
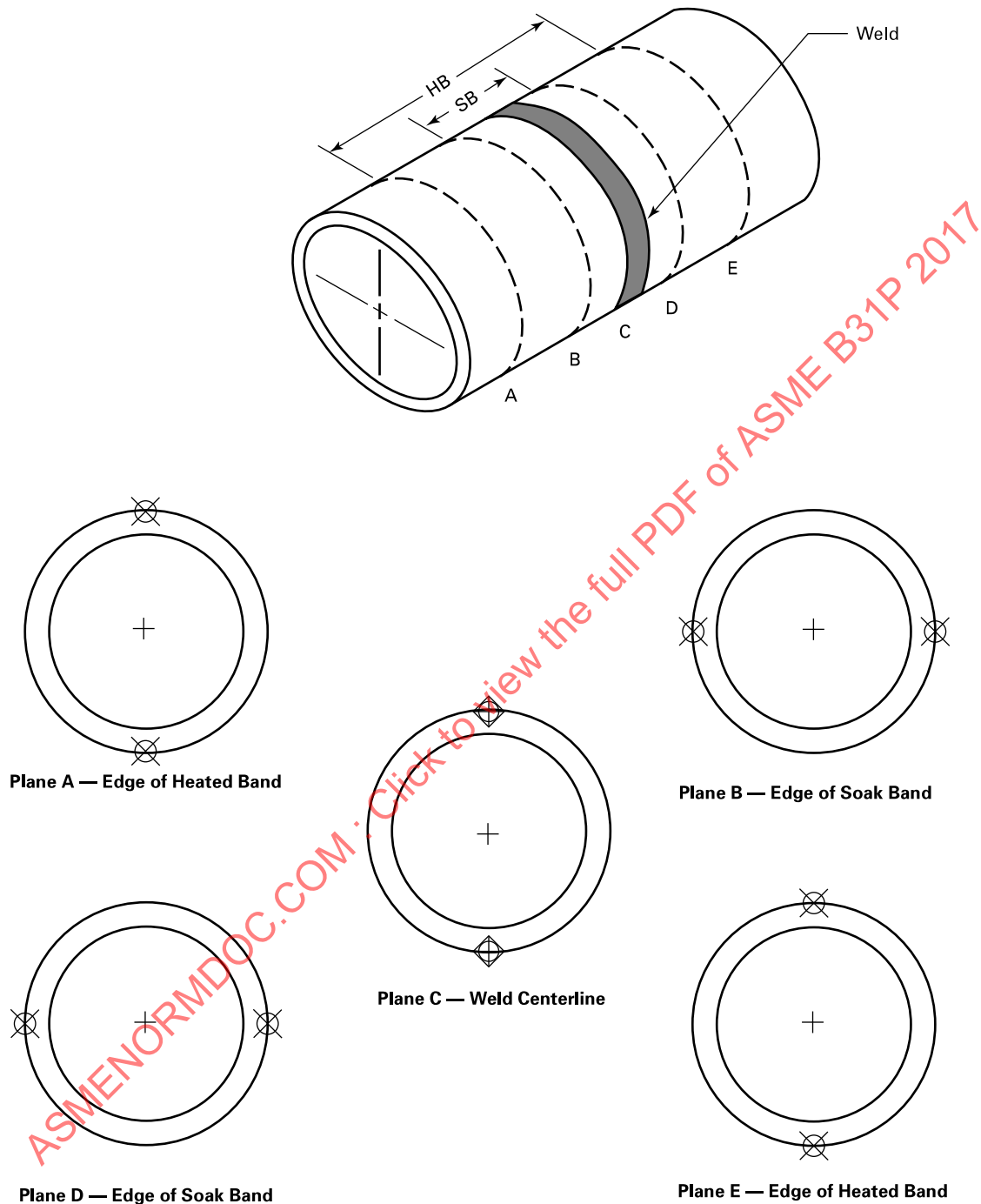


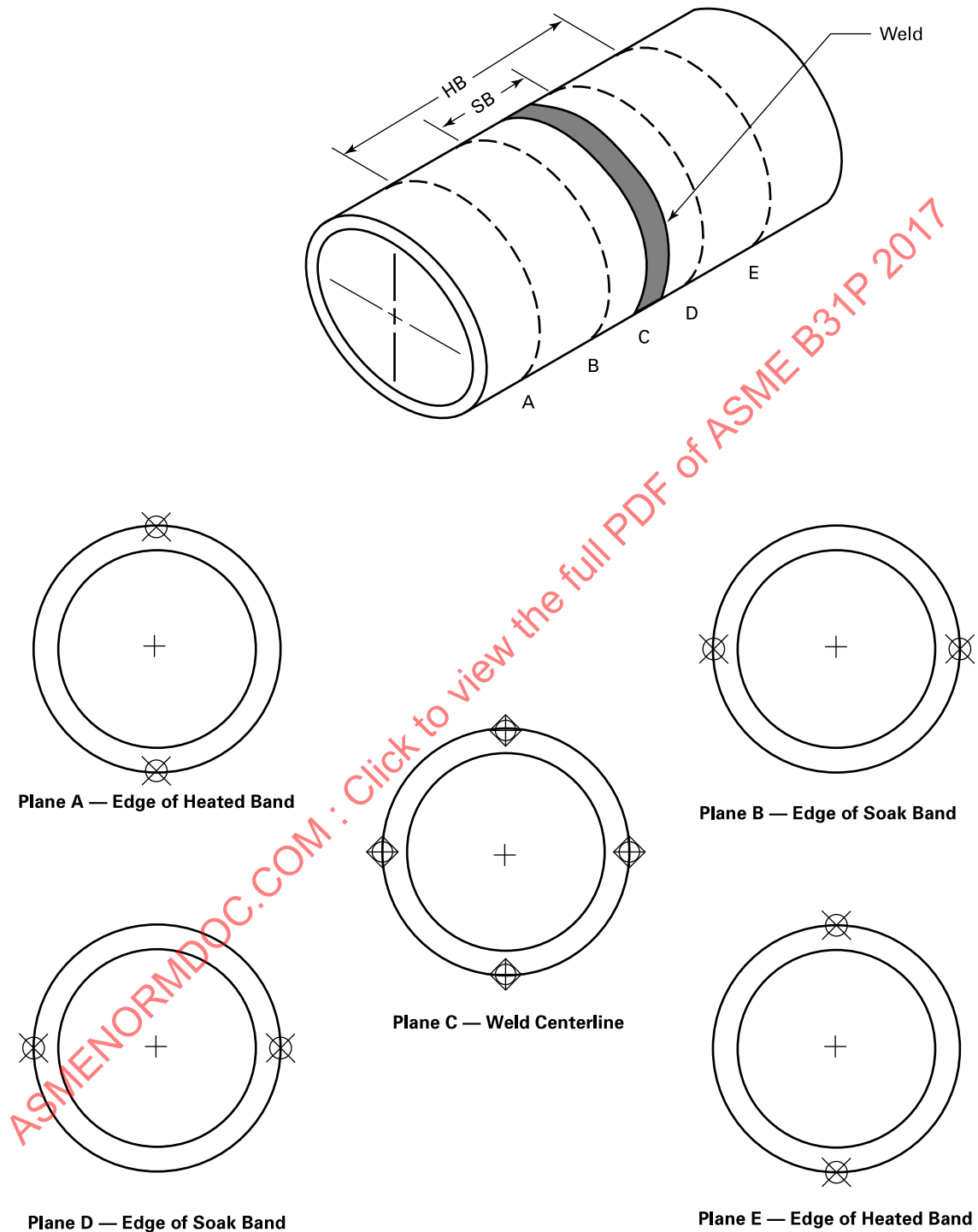
Figure B-5.2-2 Location of Thermocouples (Monitoring and Control) for Pipe Sizes NPS 6 (DN 150) Up to and Including NPS 12 (DN 300) and Two Control Zones



Legend

-  Monitoring thermocouple location on outer surface
-  Control thermocouple location on outer surface

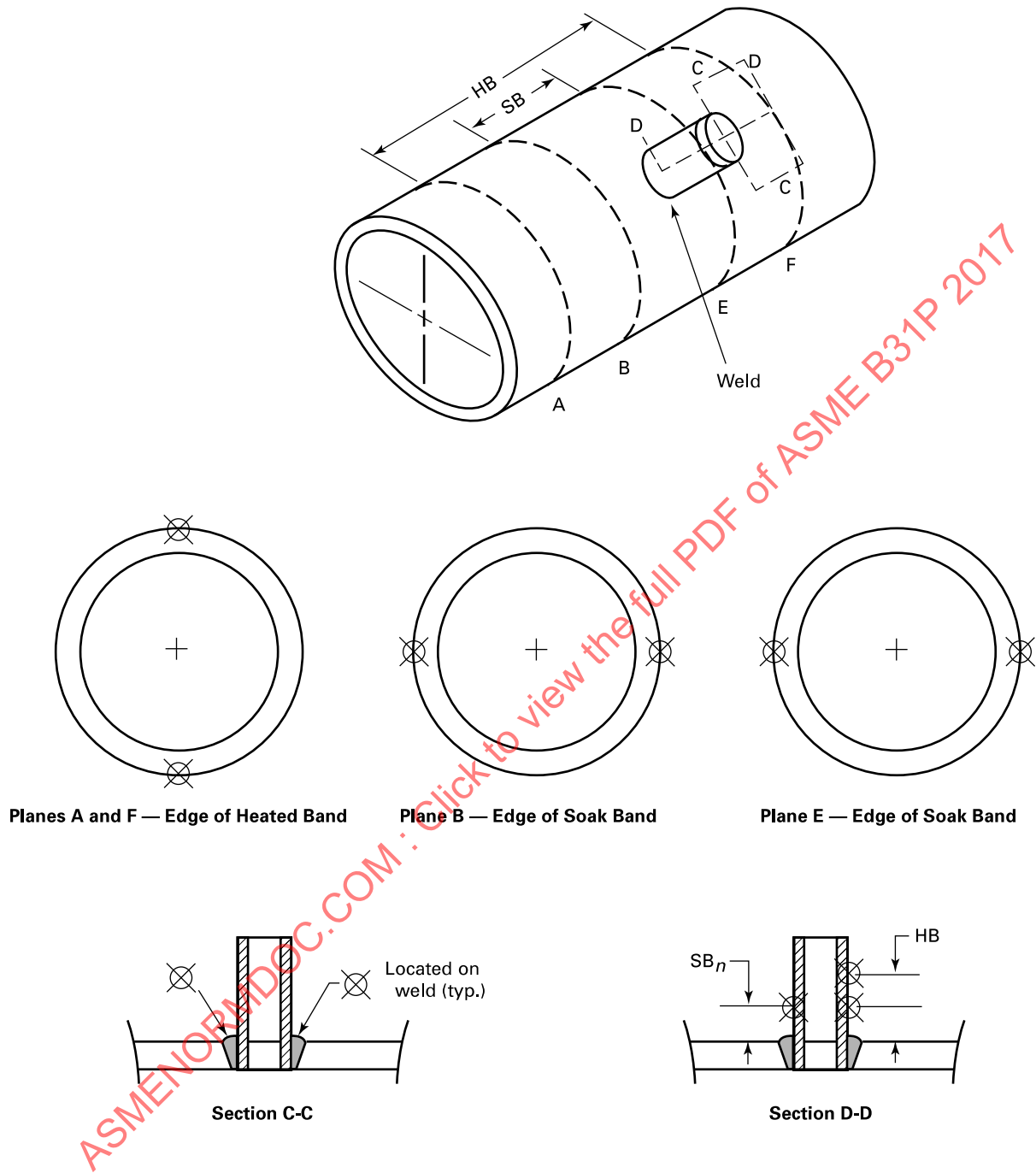
Figure B-5.2-3 Location of Thermocouples (Monitoring and Control) for Pipe Sizes NPS 14 (DN 350) Up to and Including NPS 30 (DN 750) and Four Control Zones



Legend

-  Monitoring thermocouple location on outer surface
-  Control thermocouple location on outer surface

Figure B-5.2-4 Location of Monitoring Thermocouples for Branch Nozzle or Attachment Welds



(b) *Vertical Piping.* For welds in vertical piping, the following shall be considered:

(1) Air circulation dams may be placed inside the pipe, preferably above the weld, to block the “chimney effect” within the pipe.

(2) The heated band may be biased such that approximately 60% of the heated band area is below the weld.

(3) Separate control zones, above and below the weld, may be used. Gradient control or blocking heaters may also be installed below the weld, to balance the heat flow and to form a biasing of the heated band.

(c) *Butt Welds Joining Piping to Valves and Flanges.* During PWHT of butt welds between piping and components such as valve bodies or heavy flanges, consideration shall be given to the uneven conductive heat loss on each side of the weld. In such instances, additional monitoring thermocouples shall be used to ensure that the required temperatures are achieved on both the thinner and heavier wall-thickness components. To counter the effect of different thicknesses, the heat input may be biased to the thicker side of the joint; this may be accomplished by

(1) use of separate control zones on the thicker and thinner components

(2) biasing the heating elements towards the heavier component

(3) reducing the volume of insulation used on the thinner section heated band in order to achieve the desired temperature profile across the soak band

(d) *Butt Welds Joining Branch Connections or Attachments to Piping*

(1) For welds joining branch connections or attachments to pipe, circumferential band PWHT practices shall be used on both the piping cylindrical components and the connection. The entire nozzle or attachment shall be included in the soak band.

(2) For branch connections where the heating pads fitted to the weld will not contour to the shape without leaving larger-than-normal gaps between the heaters, additional monitoring thermocouples shall be placed in the expected cold spots to ensure that the cold spots achieve the desired temperature.

(3) Where small branch connections, $\frac{1}{2}$ in. to $1\frac{1}{2}$ in. (13 mm to 38 mm) outside diameter, are welded to larger pipe sections, circumferential bands around both the larger pipe and smaller branch connection shall be heated using heaters with control thermocouples on the larger pipe and with monitoring thermocouples on the smaller branch connection. If separate control zones are used for the larger pipe and smaller branch connection, they shall each have separate control thermocouples.

(e) *Intersection With Branch Connections and Attachments Not Requiring PWHT.* The soak band, heated band, and/or gradient control band of welds that require PWHT may intersect branch connections or attachments that do not require PWHT. In order to avoid distortion and/or induced residual stresses during PWHT, the temperature gradient across the components that are intersected shall be minimized. This may require the application of a supplementary heat source(s) to the branch connection or attachment.

(1) Alternatively, a reasonably uniform temperature shall be maintained across these components. The soak band, heated band, or gradient control band, whichever intersects, shall be extended in the axial direction such that it ends beyond the weld on the opposite side connecting the attachment or associated pad to the component, for at least half of the soak band, heated band, or gradient control band, whichever is appropriate.

(2) Figure B-5.3-1 provides an example of such an approach when the heated band from a weld requiring PWHT intersects a nozzle that does not require PWHT. Note that the total distance over which the temperature drops from that at the edge of the soak band to 50% ($A + B$) is greater than or equal to $L = 2\sqrt{(Rt)}$.

(3) It should be noted that although the nonspecific term “reasonably uniform” is used to describe the temperature drop across the intersected component, the aim is to maintain a “reasonably constant” temperature drop across the intersected component. However, in order to provide a measurable limit, a maximum temperature drop is recommended as stated below.

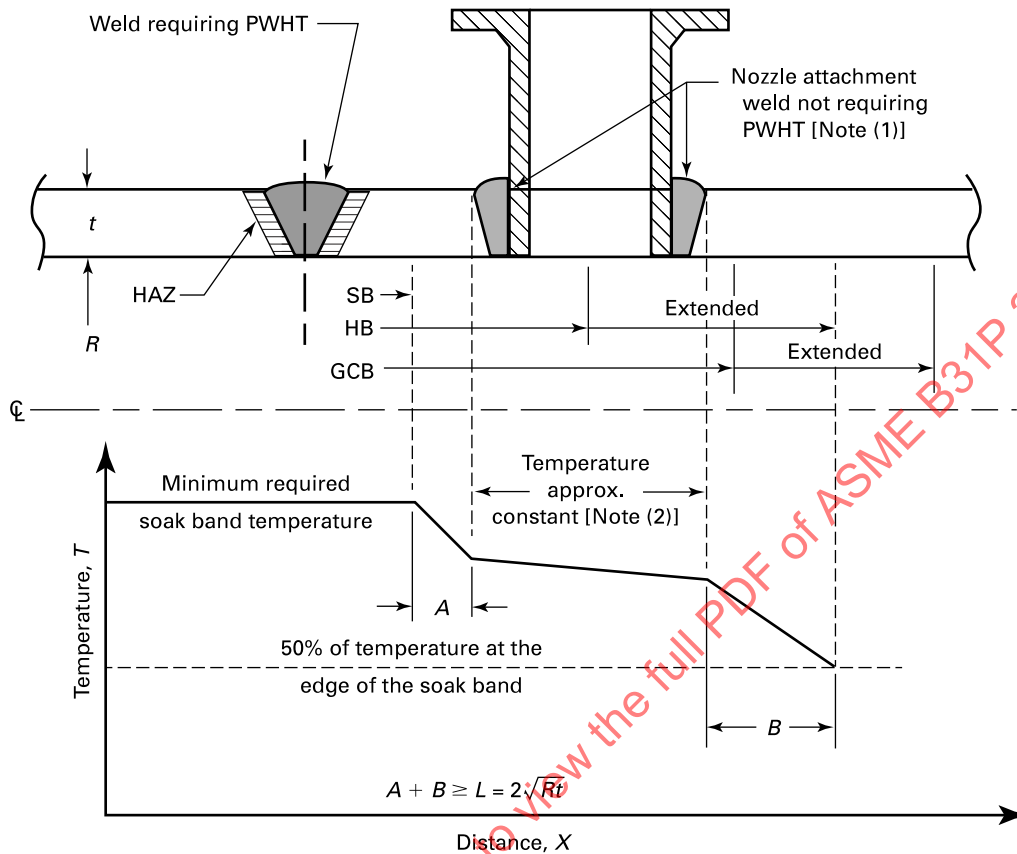
(4) The maximum temperature drop across an intersected component shall be 100°F (55°C) or that resulting from application of the maximum permissible axial temperature gradient.

(5) It is also recognized that based upon experience or analysis, larger temperature gradients across nozzles or attachments may exhibit permissible levels of distortion or residual stress.

(f) *Proximity of Pipe-to-Nozzle Welds to Shell or Head.* Consideration shall be given to whether local circumferential band PWHT of pipe-to-nozzle welds may result in heating the nozzle and/or surrounding shell or head section to temperatures that may cause distortion and harmful induced stresses.

(g) *Lower Critical Temperature (LCT) of P-No. 15E Weld Metal.* Variations in P-No. 15E weld metal chemistry are known to have a significant effect on its lower critical transformation temperature. Consideration shall therefore be given to ensuring that the upper limit of the heat-treatment temperature does not exceed the LCT of the weld metal.

Figure B-5.3-1 Example of One Approach When the Heated Band From a Weld Requiring PWHT Intersects a Weld Not Requiring PWHT



LEGEND:

- GCB = gradient control band (minimum width of insulation and/or gradient heat source)
 HB = heated band (width of heat source)
 L = minimum distance over which the temperature may drop to one-half of that at the edge of the soak band
 R = inside radius of pipe
 SB = soak band (width of the volume of the material where the holding temperature equals or exceeds the minimum and equals or is below the maximum required. The minimum width is typically specified as a multiple of t on each side of the weld.)
 t = nominal thickness of pipe

NOTES:

- (1) The nozzle attachment weld shown as "not requiring PWHT" does not imply that such a weld would not require PWHT. It simply means that it does not require PWHT now. For example, it may have previously received PWHT.
- (2) The intent is to maintain an "approximately constant" temperature across the intersected component. However, a maximum temperature drop of 100°F (55°C) or that resulting from application of the maximum recommended axial temperature gradient, whichever is less, is permitted.

B-5.4 Control of the PWHT Thermal Cycle

Four aspects of the thermal cycle associated with heating operations shall be controlled. These are temperature uniformity, the heating rate above a specified temperature, the specified hold temperature and time, and the cooling rate down to a specified temperature.

(a) *Maximum Temperature Differences for PWHT.* During heating and cooling, the maximum temperature difference within the heated band shall be 250°F (139°C) or as limited by the maximum axial temperature gradient.

(b) *Maximum Heating Rate.* The maximum heating rate shall be as specified in para. 4.2.

(c) *Maximum Hold Temperature and Time.* During hold, the requirements for the maximum hold temperature shall be as defined in Table 6.1.1-1. The hold time shall be within the requirements of the WPS if limited.

(d) *Maximum Cooling Rate.* The maximum cooling rate shall be as specified in para. 4.2.

B-5.5 Insulation

(a) *Classification of Insulation.* The requirements for the gradient control band width are based upon insulation R-values of 2°F-ft²-hr/Btu to 4°F-ft²-hr/Btu (0.35°C-m²/W to 0.70°C-m²/W). Refractory ceramic fiber insulation with a density of 6 lb/ft³ to 8 lb/ft³ (96.1 kg/m³ to 128.1 kg/m³) meets this requirement. A minimum 1 in. (25 mm) layer of insulation thickness shall be used for temperatures up to and including 1,200°F (650°C); a minimum 2 in. (50 mm) of insulation thickness shall be used for temperatures above 1,200°F (650°C).

(b) *Attachment of Insulation.* The pieces of insulation shall be sized such that when the piece(s) is wrapped around the pipe, the pipe surfaces shall be fully covered with the ends of the insulation either butted against or overlapped to preclude heat loss. No gaps shall be permitted in the insulation layer and any inadvertent gaps should be filled with insulation. The insulation may be held in place with banding or tie wire. The insulation shall not be compressed to less than three-fourths of its original thickness during banding or tying.

(c) During heating, the insulation has a tendency to shrink and, in doing so, create gaps. Inspection shall therefore be carried out at various times during the heating cycle to identify and rectify any gaps that may occur during the heating.

(d) When multiple layers of insulation are used, the seams shall be staggered to minimize the possibility of gaps.

(e) The insulation shall extend beyond the edge of the heated band out to the edge of the gradient control band, to diminish heat losses and assure that the permissible

maximum axial temperature gradient from heated to unheated sections is not exceeded.

B-5.6 Quality Requirements

(a) *Process Control.* Written procedures and associated drawings shall be used. The standard procedure for local heating shown in Form 1, or an equivalent, shall be used in conjunction with a drawing/sketch that specifies placement of thermocouples, heat sources (including control zones), and insulation.

(b) *Documentation.* A permanent record of the thermal cycle shall be produced. The temperature resolution of the record shall be to within 5°F (3°C), and the time resolution shall be to within 5 min.

(1) The record of the thermal cycle, including copies of the procedures and drawings/sketches, shall be available to the responsible organization upon the completion of local heating. The record of the thermal cycle should contain information such as the temperature and time scales and the correspondence between thermocouple numbers on the record and the drawing/sketch. The records provided may be electronic or printed copy.

(2) The standard documentation checklist for local heating shown in Form 2, or an equivalent, shall be used as a basis for provision of documentation. While the format of the checklist need not be identical, the information it includes shall be the same. This checklist, plus supporting documentation, shall be submitted to the customer at the completion of local heating.

(c) *Training.* All personnel performing local heating shall be trained in the proper use and application of the associated processes and equipment, including safety, calibration, maintenance, and inspection considerations. Each organization shall be responsible for defining its own training program, and documentation of such training shall be maintained and, if requested, made available.

B-5.7 Other Design Considerations

Additional design issues shall be considered when performing local heating of pipe. Factors that may be important during the heat treatment cycle include the following:

(a) proper support of the pipe at the strength level that will exist at the maximum temperature to be reached

(b) convection air flow within the pipe

(c) due to thermal expansion, large thermal stresses can be developed during PWHT if adequate provisions to permit thermal growth are not made

(d) the presence of internal fluids within or adjacent to the heated area