

S A E  
AERONAUTICAL INFORMATION

REPORT

NO. 18

PROPELLER SHAFT ENDS - DUAL ROTATION  
(ENGINE SUPPLIED BEARING)



DECEMBER 1, 1947

PREPARED BY

Committee E-21, Aircraft Engine Components & Accessories - Steering Committee  
Committee P-6, Propeller Standards

SOCIETY OF AUTOMOTIVE ENGINEERS, INC.  
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**REAFFIRMED**

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# PROPELLER SHAFT ENDS - DUAL ROTATION

(ENGINE SUPPLIED BEARING)

## INTRODUCTION

This report was prepared by SAE Committees E-21 and P-6 in accordance with the decisions and recommendations of the Aeronautics Committee at their meeting on January 8, 1947.

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## PROPELLER SHAFT ENDS - DUAL ROTATION

### (ENGINE SUPPLIED BEARING)

#### 1. PURPOSE:

- 1.1. It is the purpose of this report to record the results of an investigation of a dual rotation propeller shaft standard for an engine supplied bearing and the reason for deciding that such a bearing is impracticable.
- 1.2. For reference purposes the appended data and figures record the dimensions of the space considered available and the tentative requirements which were proposed for an engine supplied bearing at the time of origin May 25, 1945.

#### 2. BACKGROUND:

- 2.1. In the dual rotation engine-propeller arrangement, it is not practicable to support both shafts on bearings incorporated within the engine, because of the extreme length of the outboard shaft. Therefore, it is necessary that a bearing be incorporated near the outboard end of the inboard shaft to provide the support needed to prevent contact between the shafts under some operating loads.
- 2.2. A satisfactory propeller supplied bearing has been developed and Aeronautical Standard AS91 covering dual rotation shafts for this type of bearing has been published by the SAE and adopted by aircraft engine manufacturers. Supplementing AS91, Aeronautical Recommended Practice ARP375 has been proposed covering all involute splines and larger shaft sizes.

#### 3. CONCLUSION:

- 3.1. An engine supplied bearing seemed to offer some advantages in space and weight-saving but design studies showed the problem of supplying and sealing lubricant to such a bearing was so difficult that the engine supplied bearing was abandoned as impracticable.



| LET | TOLERANCE       |                | 40 — 60          |                  | 50 — 70          |                  | 60 — 80          |                  | 60L — 80         |                  |
|-----|-----------------|----------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
|     | OUT-BOARD SHAFT | IN-BOARD SHAFT | STRAIGHT SPLINES | INVOLUTE SPLINES | STRAIGHT SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES |
| A   | + .000          | -.002          | 3.117            | —                | 3.804            | —                | —                | —                | —                | —                |
|     | + .000          | -.005          | —                | 4.680            | —                | 5.539            | 4.680            | 6.411            | 4.680            | 6.411            |
| B   | MAX             |                | 2.875            | 4.436            | 3.554            | 5.294            | 4.436            | 6.151            | 4.436            | 6.151            |
| C   | MIN             |                | 2.783            | —                | 3.462            | —                | —                | —                | —                | —                |
|     | + .010          | -.020          | —                | 4.321            | —                | 5.179            | 4.321            | 6.036            | 4.321            | 6.036            |
| D   | ± .0008         |                | .3040            | —                | .3750            | —                | —                | —                | —                | —                |
|     | + .0000         | -.0030         | —                | .2233            | —                | .2233            | .2233            | .2233            | .2233            | .2233            |
| E   | + .000          | -.004          | 2.807            | 4.245            | 3.432            | 5.120            | 4.245            | 5.995            | 4.245            | 5.995            |
| F   | + .000          | -.005          | 2.688            | 4.062            | 3.312            | 4.938            | 4.062            | 5.812            | 4.062            | 5.812            |
| G   | + .000          | -.002          | 2.812            | 4.296            | 3.500            | 5.156            | 4.296            | 6.011            | 4.296            | 6.011            |
| H   | + .000          | -.002          | 3.125            | 4.687            | 3.812            | 5.562            | 4.687            | 6.426            | 4.687            | 6.426            |
| I   | ± .025          |                | 2.062            | 1.812            | 5.000            | 1.812            | 3.312            | 3.250            | 3.312            | 3.250            |
| J   | ± .040          |                | 2.562            | 2.312            | 5.500            | 2.312            | 3.812            | 3.750            | 3.812            | 3.750            |
| K   | ± .020          |                | 5.875            | 5.375            | 8.812            | 5.375            | 7.359            | 7.400            | 7.359            | 7.400            |
| L   | ± .030          |                | 6.000            | —                | 8.938            | —                | —                | —                | —                | —                |
| M   | + .010 - *      |                | 7.100            | 8.360            | 10.037           | 8.360            | 8.870            | 10.360           | 8.870            | 10.360           |
| N   | + .010<br>-.030 |                | 8.266            | 9.735            | 11.203           | 9.735            | 10.245           | 11.610           | 10.245           | 11.610           |
| P   | ± .020          |                | 8.938            | —                | 11.875           | —                | 10.750           | —                | 10.750           | —                |
| Q   | ± .020          |                | 7.000            | 8.250            | 9.938            | 8.250            | 8.750            | 10.250           | 8.750            | 10.250           |
| R   | MAX             |                | 1.530            | 2.030            | 1.530            | 2.030            | 2.030            | 2.030            | 2.030            | 2.030            |
|     | MIN             |                | 1.125            | 1.125            | 1.125            | 1.125            | 1.125            | 1.125            | 1.125            | 1.125            |
| r   | + .030          | -.000          | .062             | .062             | .062             | .062             | .062             | .062             | .062             | .062             |
| S   | + .0000         |                | 2.7560           | —                | 3.3810           | —                | —                | —                | —                | —                |
|     | + .0000         |                | —                | 4.1668           | —                | 5.0418           | 4.1668           | 5.9168           | 4.1668           | 5.9168           |
| T   | —               |                | 2.8125 - 12      | 4.250 - 8        | 3.4375 - 12      | 5.125 - 8        | 4.250 - 8        | 6.000 - 8        | 4.250 - 8        | 6.000 - 8        |
| U   | ± .030          |                | .170             | .250             | .170             | .250             | .250             | .250             | .250             | .250             |
| V   | APPROXIMATE     |                | —                | .068             | —                | .068             | .068             | .068             | .068             | .068             |
| X   | —               |                | 16               | 32               | 16               | 38               | 32               | 44               | 32               | 44               |
| Y   | —               |                | —                | 7/16             | —                | 7/16             | 7/16             | 7/16             | 7/16             | 7/16             |
| Z   | THEO            |                | —                | 4.5714           | —                | 5.4286           | 4.5714           | 6.2857           | 4.5714           | 6.2857           |
| CD  | MAX             |                | 4.032            |                  | 4.908            |                  | 5.782            |                  | 5.782            |                  |
| CE  | MIN             |                | 3.972            |                  | 4.843            |                  | 5.718            |                  | 5.718            |                  |
| CF  | ± .040          |                | 13.062           |                  | 13.062           |                  | 17.500           |                  | 22.500           |                  |
| CG  | —               | ± .030         | —                | 10.312           | —                | 10.312           | —                | 12.188           | —                | 12.188           |
| CH  | MAX             |                | .062             |                  | .188             |                  | .188             |                  | .188             |                  |
| DD  | —               |                | 5.812            |                  | 6.688            |                  | 7.562            |                  | 7.562            |                  |
| EE  | MAX             |                | .750             |                  | .750             |                  | .750             |                  | .750             |                  |
| FF  | —               |                | .312             |                  | .312             |                  | .312             |                  | .312             |                  |
| GG  | MIN             |                | 7.750            |                  | 8.750            |                  | 9.625            |                  | 9.625            |                  |
| HH  | ± .001          |                | 10.123           |                  | 11.123           |                  | 12.625           |                  | 12.625           |                  |
| JJ  | + .005<br>-.000 | —              | 2.188            |                  | 2.812            |                  | 3.562            |                  | 3.562            |                  |
| LL  | MIN **          |                | 2.062            |                  | 2.062            |                  | 2.062            |                  | 2.062            |                  |
| MM  | MAX             |                | 6.188            |                  | 7.062            |                  | 7.938            |                  | 7.938            |                  |
| PP  | MIN **          |                | 35°              |                  | 35°              |                  | 35°              |                  | 35°              |                  |
| QQ  | ± .025          |                | .938             |                  | .938             |                  | .938             |                  | .938             |                  |
| SS  | MIN             |                | .500             |                  | .500             |                  | .500             |                  | .500             |                  |
| TT  | ± .030          |                | 3.000            |                  | 3.000            |                  | 3.000            |                  | 3.000            |                  |
| VV  | MAX             |                | 10.102           |                  | 11.072           |                  | 12.574           |                  | 12.574           |                  |

INBOARD AXIAL DIMENSIONS ARE FROM THRUST NUT  
M DIM MAX LIMIT GIVES MIN FULL THREAD  
\* MINUS VALUE DEPENDS ON METHOD OF THREADING AND THD RUNOUT  
RELATION TO SHOULDER Q  
TO OBTAIN DIM FOR FULL NUMBER OF PITCHES, WHEN DESIRED, DEDUCT  
BASIC M FROM BASIC N  
M DIM DOES NOT APPLY WHEN UNDERCUT IS USED  
\*\* LL TO BE 4.000 AND PP TO BE 45° WHEN PRACTICABLE

TABLE FOR FIG 1 AND 2  
(PART I)

UNLESS OTHERWISE SPECIFIED  
ALLOWABLE TOLERANCE ON  
FINISHED DIMS IS ± .010  
ANGULAR DIMS IS ± 2°

| LET | TOLERANCE       |                | 41 — 60          |                  | 51 — 70          |                  | 70 — 90          |                  |  |
|-----|-----------------|----------------|------------------|------------------|------------------|------------------|------------------|------------------|--|
|     | OUT-BOARD SHAFT | IN-BOARD SHAFT | INVOLUTE SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES | INVOLUTE SPLINES |  |
| A   | + .000          | - .005         | 3.083            | 4.680            | 3.750            | 5.539            | 5.539            | 7.554            |  |
| B   | MAX             |                | 2.917            | 4.436            | 3.583            | 5.294            | 5.294            | 7.294            |  |
| C   | + .000          | - .020         | 2.850            |                  | 3.517            |                  |                  |                  |  |
|     | + .010          | - .020         |                  | 4.321            |                  | 5.179            | 5.179            | 7.179            |  |
| D   | + .0000         | - .0030        | .1299            | .2233            | .1299            | .2233            | .2233            | .2233            |  |
| E   | + .000          | - .004         | 2.807            | 4.245            | 3.432            | 5.120            | 5.120            | 7.120            |  |
| F   | + .000          | - .005         | 2.688            | 4.062            | 3.312            | 4.938            | 4.938            | 6.938            |  |
| G   | + .000          | - .002         | 2.812            | 4.296            | 3.500            | 5.156            | 5.156            | 7.156            |  |
| H   | + .000          | - .002         | 3.125            | 4.687            | 3.812            | 5.562            | 5.562            | 7.570            |  |
| I   | ± .025          |                | 2.062            | 1.812            | 5.000            | 1.812            | 3.312            | 3.312            |  |
| J   | ± .040          |                | 2.562            | 2.312            | 5.500            | 2.312            | 3.812            | 3.812            |  |
| K   | ± .020          |                | 5.875            | 5.375            | 8.812            | 5.375            | 8.188            | 8.000            |  |
| L   | ± .030          |                |                  |                  | 8.938            |                  |                  |                  |  |
| M   | + .010          | - *            | 7.100            | 8.360            | 10.037           | 8.360            | 10.360           | 11.610           |  |
| N   | + .010          | - .030         | 8.266            | 9.735            | 11.203           | 9.735            | 11.735           | 13.110           |  |
| P   | ± .020          |                | 8.938            |                  | 11.875           |                  | 12.375           |                  |  |
| Q   | ± .020          |                | 7.000            | 8.250            | 9.938            | 8.250            | 10.250           | 11.500           |  |
| R   | MAX             |                | 1.530            | 2.030            | 1.530            | 2.030            | 2.030            | 2.030            |  |
|     | MIN             |                | 1.125            | 1.125            | 1.125            | 1.125            | 1.125            | 1.125            |  |
| r   | + .030          | - .000         | .062             | .062             | .062             | .062             | .062             | .062             |  |
| S   | + .0000         | - .0030        | 2.7560           |                  | 3.3810           |                  |                  |                  |  |
|     | + .0000         | - .0050        |                  | 4.1668           |                  | 5.0418           | 5.0418           | 7.0418           |  |
| T   |                 |                | 2.8125 - 12      | 4.250 - 8        | 3.4375 - 12      | 5.125 - 8        | 5.125 - 8        | 7.125 - 8        |  |
| U   | ± .030          |                | .170             | .250             | .170             | .250             | .250             | .250             |  |
| V   | APPROXIMATE     |                | .035             | .068             | .035             | .068             | .068             | .068             |  |
| X   |                 |                | 36               | 32               | 44               | 38               | 38               | 52               |  |
| Y   |                 |                | 12/24            | 7/16             | 12/24            | 7/16             | 7/16             | 7/16             |  |
| Z   | THEO            |                | 3.0000           | 4.5714           | 3.6667           | 5.4286           | 5.4286           | 7.4286           |  |
| CD  | MAX             |                | 4.032            |                  | 4.908            |                  | 6.908            |                  |  |
| CE  | MIN             |                | 3.972            |                  | 4.843            |                  | 6.593            |                  |  |
| CF  | ± .040          |                | 13.062           |                  | 13.062           |                  | 25.000           |                  |  |
| CG  |                 | ± .030         |                  | 10.312           |                  | 10.312           |                  | 13.750           |  |
| CH  | MAX             |                | .062             |                  | .188             |                  | .219             |                  |  |
| DD  |                 |                | 5.812            |                  | 6.688            |                  | 8.750            |                  |  |
| EE  | MAX             |                | .750             |                  | .750             |                  | 1.000            |                  |  |
| FF  |                 |                | .312             |                  | .312             |                  | .312             |                  |  |
| GG  | MIN             |                | 7.750            |                  | 8.750            |                  | 11.375           |                  |  |
| HH  | ± .001          |                | 10.123           |                  | 11.123           |                  | 14.373           |                  |  |
| JJ  | + .005          | - .000         | 2.188            |                  | 2.812            |                  | 4.375            |                  |  |
| LL  | MIN             |                | 2.062 **         |                  | 2.062 **         |                  | 4.0000           |                  |  |
| MM  | MAX             |                | 6.188            |                  | 7.062            |                  | 9.125            |                  |  |
| PP  | MIN             |                | 35° **           |                  | 35° **           |                  | 45°              |                  |  |
| QQ  | ± .025          |                | .938             |                  | .938             |                  | .938             |                  |  |
| SS  | MIN             |                | .500             |                  | .500             |                  | .500             |                  |  |
| TT  | ± .030          |                | 3.000            |                  | 3.000            |                  | 3.000            |                  |  |
| VV  | MAX             |                | 10.102           |                  | 11.072           |                  | 14.250           |                  |  |

INBOARD AXIAL DIMENSIONS ARE FROM THRUST NUT  
M DIM MAX LIMIT GIVES MIN FULL THREAD  
\* MINUS VALUE DEPENDS ON METHOD OF THREADING AND THD RUNOUT  
RELATION TO SHOULDER Q  
TO OBTAIN DIM FOR FULL NUMBER OF PITCHES, WHEN DESIRED, DEDUCT  
BASIC M FROM BASIC N  
M DIM DOES NOT APPLY WHEN UNDERCUT IS USED  
\*\* LL TO BE 4.000 AND PP TO BE 45° WHEN PRACTICABLE

TABLE FOR FIG 1 AND 2  
(PART II)

UNLESS OTHERWISE SPECIFIED  
ALLOWABLE TOLERANCE ON  
FINISHED DIMS IS ± .010  
ANGULAR DIMS IS ± 2°